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# (54) 【発明の名称】 撥水性ガラスおよびその製造方法

# (57)【要約】

【目的】 保存安定性に優れた挽水挽油液を用い、簡単な積層膜構成で、挽水性能はもとより、より長期的に耐摩耗性、耐候性に優れた挽水性ガラスを得る。

【構成】 ガラス基板と、該基板の表面に、表面処理することなく成膜した状態でマイクロビット状表層、凹凸状表層、凸状表層のうち少なくとも1種以上の表層形状を呈している酸化物薄膜あるいは混合酸化物薄膜で成る下地層と、該下地層の上に、少なくともフルオロアルキルシラン0.1~20重量%と、酸化アンチモンをドーパントとする酸化錫の粒子0.04~2重量%と、シリコーン化合物0.03~2重量%と、水を0.005~15重量%と、有機溶媒からなる混合溶液に、酸をフルオロアルキルシラン1mol に対して5×10-4mol ~2×10-2mol になるよう添加した飛水税油液を塗布成膜した薄膜である飛水層とからなることを特徴とする飛水性ガラス。並びにその製造方法。

## 【特許請求の範囲】

【請求項1】 ガラス基板と、該基板の表面に、表面処理することなく成膜した状態でマイクロピット状表層、凹凸状表層、凸状表層のうち少なくとも1種以上の表層形状を呈している酸化物薄膜あるいは混合酸化物薄膜で成る下地層と、該下地層の上に、少なくともフルオロアルキルシラン0.1~20重量%と、酸化アンチモンをドーパントとする酸化鍋の粒子0.04~2重量%と、シリコーン化合物0.03~2重量%と、水を0.005~15重量%と、有機溶媒からなる混合溶液に、酸をフルオロアルキルシ 10ラン1 mol に対して5×10-4 mol ~2×10-2 mol になるよう添加した飛水挽油液を塗布成膜した薄膜である挽水層とからなることを特徴とする飛水性ガラス。

【請求項2】 前記酸化物薄膜あるいは混合酸化物薄膜で成る下地層が、平均膜厚として10~300nmであって、マイクロビット状表層、凹凸状表層、凸状表層のうち少なくとも1種以上の表層形状として R max (最大高さ) = 5~60nm、R a (中心線平均粗さ) = 2~20nm、R x (10点平均粗さ) = 5~55nm、S a (凹凸の平均間隔) = 5~700nmで成ることを特徴とする請求項1記載の税水性ガラス。

【請求項3】 前記酸化物薄膜あるいは混合酸化物薄膜で成る下地層が、マイクロピット状表層、凹凸状表層、 凸状表層のうち少なくとも1種以上の表層形状としてスキューネス(歪度)=0乃至>0、クルトシス(失度) =3乃至>3であることを特徴とする請求項1乃至2記 載の飛水性ガラス。

【請求項4】 少なくともフルオロアルキルシラン0.1~20重量%と、酸化アンチモンをドーパントとする酸化 錫の粒子0.04~2重量%と、シリコン化合物0.03~2重量%と、水を0.005~15重量%および有機溶媒とからなる混合溶液に、酸をフルオロアルキルシラン1 mol に対して5×10-4 mol ~2×10-2 mol になるように添加した 焼水焼油液を、酸化物溶液あるいは混合酸化物溶液を被膜し、550~650 ℃で焼成後においてもそのまま、マイクロビット状表層、凹凸状表層、凸状表層のうち少なくとも1種以上の表層形状を呈している酸化物膜あるいは混合酸化物薄膜を下地層として設けたガラス基板の下地層上に塗布し、次いで100~400 ℃で焼き付けることを特徴とする焼水性ガラスの製造方法。

【請求項5】 前記酸化物薄膜あるいは混合酸化物薄膜で成る下地層が、平均膜厚として10~300nmであって、マイクロピット状表層、凹凸状表層、凸状表層のうち少なくとも1種以上の表層形状として R max (最大高さ) = 5~60nm、R a (中心線平均粗さ) = 2~20nm、R z (10点平均粗さ) = 5~55nm、S m (凹凸の平均間隔) = 5~700nmであるマイクロピット状表層、凹凸状表層、凸状表層のうち少なくとも1種以上でなるようにしたことを特徴とする請求項4記載の挽水性ガラスの製造方法。

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【請求項6】 前記酸化物薄膜あるいは混合酸化物薄膜で成る下地層が、マイクロピット状表層、凹凸状表層、凸状表層のうち少なくとも1種以上の表層形状としてスキューネス(歪度)=0乃至>0、クルトシス(尖度)=3乃至>3であるようにしたことを特徴とする請求項4乃至5記載の飛水性ガラスの製造方法。

【発明の詳細な説明】

[0001]

【産業上の利用分野】本発明は、挽水挽油性能はもとより、耐久性、耐摩耗性に優れた撓水性ガラスおよびその 製造方法に関し、車両用、船舶用、航空機用あるいは建 築用等のウィンドウガラスやミラーなどに有用である。 【0002】

【従来技術】ガラスや樹脂等の基材に飛水挽油性を付与させるために、フルオロアルキル基含有化合物やジメチルシロキサン、フッ素系樹脂を含有する処理剤を前記基材表面に塗布成膜する試みがなされている。しかしこれらの処理剤を単に塗布しただけでは前記基材表面との結合力が弱く、耐候性や耐摩耗性を充分にもたせることはできず、飛水性を長期に亘り維持することは困難であった。

【0003】これまでは、ガラスなどの素材上に、挽水 廃油性を付与するためにポリフルオロアルキル基(Rf 基)含有シラン化合物とアルコール等の希釈剤を用いた ものが各種出願されている。例えば特開昭58-122979号 公報、特開昭58-129082号公報、特開昭58-172245号公 報、特開平5-345641号公報等である。

【0005】また例えば、特開昭58-167448号公報には、ポリフルオロアルキル基含有シラン化合物叉は該化合物の部分加水分解縮合物からなる厚さ1μ 以下の薄膜をガラス表面に形成することにより、透視性等を損なりことなく、低反射率及び挽水税油性とする低反射率ガラスが記載されている。

【0006】しかし、このような従来の処理剤を用いた 挽水挽油処理では、基材表面に導入される挽水挽油基の 結合力が弱く、耐久性、耐候性試験において、比較的短 時間で挽水性が劣化し、挽水性能を長く持続することが できないという問題点があった。

【0007】さらに耐候性に優れたものとして、テフロンを被覆したガラスがあるが、膜が柔らかいため傷つき易くすぐに透明性が損なわれるという問題点があった。

50 また例えば、特開昭60-231442号公報には、ガラス基板

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上に接着成分としてシロキサン結合を有する有機ケイ素化合物の重合物、および税水成分としてフッ素化合物の重合物の双方よりなる税水性被膜を形成した税水処理硝子が記載されているが、表面が税水成分の重合物が全てまたは相対的に多く含有された構成になっているために傷つき易いという問題点があった。

【0008】また例えば、特開平3-153859号公報には、プラスチック基板上に金属酸化物層が形成され、その上に金属酸化物層およびフッ素樹脂の複合層を積層した表面改質プラスチックが記載されているが、基板がプ 10ラスチックであるため密着性が必ずしも満足できるものではない等の問題がある。

【0009】また例えば、特開平5-51238 号公報には、ガラス基板上に金属酸化物相と該金属酸化物相中に分散された税水性微粒子とからなる税水層をもつ税水性ガラスが記載されているが、微粒子が均等に膜中に分散した構成では傷つき易いという問題点があった。

【0010】また例えば特開平4-160039号公報には、 ガラス表面に金属酸化物被膜を設け、更にその表面に、 SnやSbの元素のイオンをイオン注入することにより競水 20 性を付与することが記載されているが、充分な初期接触 角が得られないことや注入後にイオンが徐々に酸化し挽 水性能が長く持続できないという問題点があった。

【0011】また、基材表面に下地層と挽水層を設けたものとしては、例えば特開平2-311332号公報には、ガラス基材表面にSiO、等の金属酸化物層を形成し、アルコキシシラン化合物及びフルオロアルキルシラン化合物等のシリル化した飛水層を設ける挽水性ガラスの製造方法が記載されており、さらに特開平5-238781号公報には、ガラス基体表面にシリカ下地層、及びペルフルオロアルキル、アルキルシランで処理されている耐久挽水性表面を有するガラス物品が記載されている等がある。これらでは特に過酷な環境下での長期的な耐久性や耐摩耗性等において挽水性の劣化や微小な傷が微かに付くようなことがあり、必ずしも充分とは言い難いものであった。

【0012】またさらに基板表面に凹凸状の下地層を設け、その上に飛水層を設けたものとしては、例えば特開平4-124047号公報には、硝子表面に金属酸化物皮膜を形成し、エッチングによって凹凸を設け、その上にポリ 40フルオロアルキル基を有するフッ素シリコン等の飛水処理剤をコーティングするガラス表面の飛水処理方法が記載されており、さらにまた特開平6-116430号公報には、プラスチックフイルム上に微小な凹凸(粗さが0.01~0.3 μm)を形成した(プラズマ放電処理)SiO2等の無機硬質膜と、この上にシロキサン結合を介して形成させたフッ素を含む化学吸着単分子膜とからなる飛水飛油性フイルムが記載されている等がある。これらはいずれもその凹凸処理が複雑であり、凹凸形状も所期のものとは異なり、しかも特により過酷な環境下での飛水性の長 50

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## [0013]

【発明が解決しようとする問題点】本発明は上記従来の問題点を解決するものであり、その目的は、密着性、耐候性に優れしかも硬い、特により過酷な環境下での飛水性能の長期的な耐久性や耐摩耗性等を維持できる飛水性ガラスおよびその製造方法を、特異な形成による特異な形状の下地層と保存安定性に優れた特定した飛水焼油液の組み合わせ積層することによって提供することにある。

#### [0014]

【問題点を解決するための手段】本発明は、従来のかかる問題点に鑑みてなされたものであって、少なくともフルオロアルキルシラン0.1~20重量%と、酸化アンチモンをドーパントとする酸化錫の粒子0.04~2重量%と、シリコン化合物0.03~2重量%と、水を0.005~15重量%および有機溶媒とからなる混合溶液に、酸をフルオロアルキルシラン1molに対して5×10<sup>-4</sup>mol~2×10<sup>-2</sup>molになるように添加した特定の提水焼油液を、酸化物溶液あるいは混合酸化物溶液を被膜し、550~650℃で焼成後においてもそのまま、マイクロビット状表層、凹凸状表層、凸状表層のうち少なくとも1種以上の表層形状を呈している酸化物膜あるいは混合酸化物薄膜を下地層として設けたガラス基板の下地層上に塗布し、次いで100~400℃で焼き付けることにより、上記目的が達成できる。

【0015】また本発明は、ガラス基板と、該基板の表面に、表面処理することなく成膜した状態でマイクロピット状表層、凹凸状表層、凸状表層のうち少なくとも1種以上の表層形状を呈している酸化物薄膜あるいは混合酸化物薄膜で成る下地層と、該下地層の上に、少なくともフルオロアルキルシラン0.1~20重量%と、酸化アンチモンをドーパントとする酸化錫の粒子0.04~2重量%と、シリコーン化合物0.03~2重量%と、水を0.005~15重量%と、有機溶媒からなる混合溶液に、酸をフルオロアルキルシラン1mol に対して5×10-4mol ~2×10-2mol になるよう添加した飛水飛油液を塗布成膜した薄膜である飛水層とからなることを特徴とする飛水性ガラスを提供する。

【0016】また本発明は、ガラス基板と、該基板の表面に、前記したマイクロピット状表層、凹凸状表層、凸状表層のうち少なくとも1種以上の表層形状を呈している酸化物薄膜あるいは混合酸化物薄膜における該マイクロピットまたは/および凹凸あるいは/ならびに凸が、Reax(最大高さ)=5~60nm、Ra(中心線平均粗さ)=2~20nm、Rx(10点平均粗さ)=5~50nm、Sa(凹凸の平均間隔)=5~700nmであることから成る

膜厚が10~300mmの下地層と、該下地層の上に、前記した機水搬油液を塗布成膜した薄膜である機水層とからなることを特徴とする搬水性ガラスを提供する。

【0017】また本発明は、ガラス基板と、該基板の表面に、前記したマイクロピット状表層、凹凸状表層、凸状表層のうち少なくとも1種以上の表層形状を呈している酸化物薄膜あるいは混合酸化物薄膜における該マイクロピットまたは/および凹凸あるいは/ならびに凸が、スキューネス(歪度)=0乃至>0、クルトシス(失度)=3乃至>3であることから成る下地層と、該下地層の上に、前記した飛水税油液を塗布成膜した薄膜である飛水層とからなることを特徴とする飛水性ガラスを提供する。

【0018】また本発明は、ガラス基板と、該基板の表面に、前記したマイクロピット状表層、凹凸状表層、凸状表層のうち少なくとも1種以上の表層形状を呈している酸化物薄膜あるいは混合酸化物薄膜における該マイクロピットまたは/および凹凸あるいは/ならびに凸が、Rmax(最大高さ)=5~60mm、Ra(中心線平均粗さ)=5~55mm、S20a(凹凸の平均間隔)=5~700mmであることから成り、しかもスキューネス(歪度)=0乃至>0、クルトシス(尖度)=3乃至>3であることから成る下地層と、該下地層の上に、前記した飛水焼油液を塗布成膜した薄膜である飛水層とからなることを特徴とする焼水性ガラスを提供する。

【0019】また本発明は、前記した挽水挽油液を、平均膜厚として10~300nmであって、R max(最大高さ)=5~60nm、R a (中心線平均粗さ)=2~20nm、R z (10点平均粗さ)=5~55nm、S a (凹凸の平均間隔)=5~700nmであるマイクロピットまたは/および凹凸あるいは/ならびに凸を有するマイクロピット状表層、凹凸状表層、凸状表層のうち少なくとも1種以上でなる前記した酸化物膜あるいは混合酸化物薄膜を下地層として設けたガラス基板の下地層上に塗布し、次いで100~400℃で焼き付けることを特徴とする挽水性ガラスの製造方法を提供する。

【0020】また本発明は、前記した税水税油液を、スキューネス(歪度)=0乃至>0、クルトシス(尖度)=3乃至>3であるマイクロピットまたは/および凹凸 40あるいは/ならびに凸のマイクロピット状表層、凹凸状表層、凸状表層のうち少なくとも1種以上でなる前記した酸化物膜あるいは混合酸化物薄膜を下地層として設けたガラス基板の下地層上に塗布し、次いで100~400℃で焼き付けることを特徴とする税水性ガラスの製造方法を提供する。

【0021】また本発明は、前記した撥水撥油液を、平均膜厚として10~300nmであって、R max (最大高さ) = 5~60nm、R a (中心線平均粗さ) = 2~20nm、R a (10点平均粗さ) = 5~55nm、S a (凹凸の平均間

隔)=5~700mであり、しかもスキューネス(歪度) =0乃至>0、クルトシス(尖度)=3乃至>3である マイクロビットまたは/および凹凸あるいは/ならびに 凸のマイクロビット状表層、凹凸状表層、凸状表層のう ち少なくとも1種以上でなる前記した酸化物膜あるいは 混合酸化物薄膜を下地層として設けたガラス基板の下地 層上に塗布し、次いで100~400℃で焼き付けることを

特徴とする脱水性ガラスの製造方法を提供する。

スキューネス(歪度)=0乃至>0、クルトシス(失度)=3乃至>3であることから成る下地層と、該下地 10 層の上に、前記した税水税油液を塗布成膜した薄膜である税水層とからなることを特徴とする税水性ガラスを提供する。
【0018】また本発明は、ガラス基板と、該基板の表面に、前記したマイクロピット状表層、凹凸状表層、凸状表層のうち少なくとも1種以上の表層形状を呈している酸化物薄膜あるいは混合酸化物薄膜における該マイクロピットまたは/および凹凸あるいは/ならびに凸が、 【0022】ここで、前記ガラス基板としては、無機質の透明板ガラスであって、車輌用、船舶用、航空機用あるいは建築用等に用いられる市販のソーダライムガラスを採用することができ、無色または着色、ならびにその種類あるいは色調、形状等にとくに限定されるものではなく、さらに曲げ板ガラスとしてはもちろん、各種強化ガラスや強度アップガラス、平板や単板で使用できるととに、複層ガラスあるいは合せガラス、またミラー用がラスとしても使用できることは言うまでもないものである。

【0023】また前記した下地層とする酸化物膜として は、いかなる手法により作製してもよいが、例えば金属 アルコキシド系化合物あるいは金属アセチルアセトネート系化合物中から少なくとも1種以上の化合物を2つ以上選択し、しかも該選択した該溶液の選択する2つ以上の化合物の混合割合の調整または/および該溶液を相対 湿度のコントロールのもとに成膜し、100 ℃以上の温度で加熱することにより得ることができる。該下地層の成膜は、100 ~300 ℃で約10分間前後によるゲル膜とした後、さらに約600 ℃前後、例えば500 ~650 ℃程度で約3分間前後焼成することが優れた耐候性や耐摩耗性等を 30 得るために好ましいものである。

【0024】ことに表面処理をすることなく前記したマイクロピット状表層、凹凸状表層、凸状表層のうち少なくとも1種以上の表層形状を呈している酸化物薄膜となり、さらに550~650℃程度で焼成しても被膜乾燥時のマイクロピット状表層、凹凸状表層、凸状表層のうち少なくとも1種以上の表層形状が崩れるようなことがない。以下の下地層でも同様である。

【0025】上述した選択した2つ以上の化合物については、例えば平均分子量が異なるものを選択し、該選択は成膜した酸化物膜の表層をマイクロビット状、凹凸状あるいは凸状とするためであり、混合する2種以上の化合物の平均分子量は数千(具体的には例えば800 乃至800程度、好ましくは2000乃至7000程度)と数万(具体的には例えば10000 乃至70000程度)あるいは、数千と数十万(具体的には例えば100000万至400000程度)の組み合わせであることが好ましい。

【0026】さらに下地層としては、例えば一つの出発 原料として4官能を有する金属アルコキシドあるいは金 属アセチルアセトネート化合物を加水分解ならびに脱水 50 縮合したゾル溶液Aと、さらに一つの出発原料として3 官能あるいは2官能を有する金属アルコキシドあるいは 金属アセチルアセトネート化合物を加水分解ならびに脱 水縮合したゾル溶液Bをそれぞれ選択し混合することな るコーティング溶液を被膜し成膜したゾルゲル膜であっ てもよいものである。

【0027】さらにまた例えば、上述したゾル溶液AおよびBとは異種金属の金属アルコキシドあるいは金属アセチルアセトネート化合物を出発原料として加水分解ならびに脱水縮合したゾル溶液Cを用い、前記ゾル溶液A、BならびにCをそれぞれ少なくとも選択し混合する10ことなるコーティング溶液を被膜し成膜したゾルゲル膜であってもよいものである。

【0028】また、上述した金属アルコキシド系化合物としては、金属にすべてアルコキシ基のみが結合した場合、すなわちメトキシド、エトキシド、イソプロボキシド等のみならず、その一部がメチル基、エチル基等に置換したもの、例えばモノメチルアルコキシド、モノエチルアルコキシド等を含むものである。さらにまた、上述した金属アセチルアセトネート系化合物としては、金属に全てアセチルアセトン基のみが結合した場合のみならが、その一部がメチルアルコキシ基、エチルアルコキシ基等に置換したものを含むものである。

【0029】さらに、上述の金属としては、とくに限定するものではないが、Si、TiまたはZrを選択するのが好ましく、具体的なものとしては、例えばテトラメトキシシラン [Si (OMe)4 Me:CH3 ] (以下MeはClb である)、テトラエトキシシラン [Si (OEt)4 Et:C2 H5 ] (以下EtはC2H5である)、メチルトリエトキシシラン [MeSi (OEt)3 ]、メチルトリメトキシシラン [MeSi (OMe)3 ]、チタン 30 テトライソプロポキシド [Ti (O-iso-Pr)4

Pr:C3 H7](以下PrはC3H7である)、チタンアセチルアセトネート「Ti(CH2 COCH2 COCH3), J、ジルコニウムノルマルブトキシド(Zr(O-n-Bu), Bu:C4 H9](以下BuはC4H5である)、ジルコニウムアセチルアセトネート「Zr(CH2 COCH2 COCH3), J等が好適であり、他に例えばジメチルジエトキシシラン、ジメチルジメトキシシラン、チタンテトラノルマルブトキシド、ジルコニウムテトライソプロポキシド、ジルコニウムテトライソプロポキシド、ジルコニウムテトラオクチレート等がある。

【0030】またさらに、前記マイクロビット状表層、 凹凸状表層、凸状表層のうちの少なくとも1種以上でな る酸化物膜あるいは混合酸化物薄膜の具体的なものとし ては、SiO2の酸化物膜、SiO2・TiO2あるいはSiO2・ZrO2 等の混合酸化物膜等が挙げられる。

【0031】また、前記マイクロピット状表層、凹凸状表層、凸状表層のうちの少なくとも1種以上でなる酸化物膜あるいは混合酸化物薄膜の下地層の平均膜厚としては10~300mであるとしたのは、10nm未満では所期の表

層形状が得られ難くなって撓水剤の充分な量の保持がで きなくなり、長期の飛水性発現ができなくなるためであ

る。また300mmを超えると経済的でなくなることはもちろん、下地層自体の物理的耐久性が低減することとなるため等である。最適には30~200mm 程度である。

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【0032】また、前記したマイクロピット状表層、凹 凸状表層、凸状表層のうち少なくとも1種以上の表層形 状を呈している酸化物薄膜あるいは混合酸化物薄膜にお ける該マイクロビット状または/および凹凸状あるいは /ならびに凸状が、 R max (最大高さ) = 5~60nm、 R a (中心線平均粗さ) = 2~20nm、R z (10点平均粗 さ) = 5~55mm、Sm(凹凸の平均間隔) = 5~700mm で成ることとしたのは、該マイクロピット状表層、凹凸 状表層、凸状表層のうち少なくとも1種以上の表層形状 のマイクロビット状または/および凹凸状あるいは/な らびに凸状を表現することは困難であるが、走査型プロ ーブ顕微鏡のAFM モード (セイコー電子製、SP3700、4 μm四方スキャンあるいはオリンパス製、NV2000、4μ m四方スキャン)で観察し、JIS B 0601における表面粗 さの表示であるR max 、R a 、 R z さらにS m でもって 大まかに表示したものであり、例えば R max >60nm、 R a>20nm、Rょ>55nmでは摩擦などの外的な応力によ り、凹凸形状が破壊され易くなり、長期の物理的耐久性 が低減し、Raax<5mm、Ra>2mm、Rz>5mmでは ほとんど平滑状に近いものとなり到底所期のめざす表層 形状とはならないためである。

【0033】さらに、前記マイクロピット状または/および凹凸状あるいは/ならびに凸状をスキューネス(Skewness=Rsk、歪度)=0乃至>0、クルトシス(Kurtosis=Rkr、尖度)=3乃至>3であることとしたのは、スキューネスが断面(振幅分布)曲線における縦倍率方向の対称性を表す値であって、機械加工面程度である所謂Rsk=0から中心線より上に尖った円錐状の山が無平坦で多在する所謂Rsk>0の範囲の表面相さであり、平坦部のなかに深い谷が点在する(マイナスが大きいほど山がない状態)所謂Rsk<0では充分な量の挽水剤を下地層に保持しできないため、長期の挽水性発現ができなくなるものである。好ましくは0乃至0に比較的近い>0の範囲であって、細く尖りすぎて物理的耐久性が低減しない程度に尖った円錐状の山が無平坦で多在する状態の前記表層である。

【0034】またクルトシスが断面(振幅分布)曲線における形状を表す値(表面粗さの確率密度分布:正規分布に近いものが機械加工面であって Rsk=0、 Rkr=3であり、一般に形状が鋭いほど、横倍率方向の平坦部分の割合が大きい表面)であって、正規分布の山が細く尖り過ぎるような異常に高い山や深い谷がある所謂 Rkr>3では、長期の物理的耐久性が低減したり長期の飛水性発現ができなくなり、また正規分布の山が広く低くお碗50状のようなどちらかと言えば平坦状のなかにクレーター

状が点在する所謂 Rkr<3では、結果的に飛水剤との接 触面積が減り、多在する円錐状山にのめり込みながら被 覆するとは異なって飛水剤の保持が弱くなり、長期の飛 水性発現ができなくなるものであり、 Rkr=3から Rkr >3の範囲である.好ましくは Rkr=3から3に比較的 近い Rkr>3の範囲であって、適度に尖った円錐状の山 が無平坦で乱立多在する状態の前記表層である。

【0035】ことに、従来の有機溶液よりの酸化物膜を 弗酸処理するエッチングした膜、例えばSiO2膜では、R sk<0で Rkr<3となり、上述したように期待する程充 10 工業(株))がある。 分な量の飛水剤をエッチングSiOz膜に保持することがで きないため、エッチングSiOz膜がない場合よりよいもの の、めざす長期の飛水性発現ができなくなる。

【0036】これらのことから、Rsk がO乃至>0、Rk r が3乃至>3、好ましくはRsk が0乃至0に比較的近 い>0、Rkr がRkr = 3から3に比較的近い Rkr>3で あることにより、下地層として広い表面積と適度の深さ ならびに形状を有するため、充分な挽水剤の保持が可能 であるとともに、摩擦などに対する充分な物理的強度を 有するものとなるものである。

【0037】また、前記表層におけるマイクロピット 状、凹凸状あるいは凸状の大きさは、例えば成膜する際 の相対湿度により、その径を5乃至500nm に制御するこ とができる。径が500nm を超えると、酸化物膜自体の透 明性が損なわれ白化するとともに膜強度も弱くなり、ま た5nm未満では酸化錫あるいは酸化アンチモンをドーパ ントとする酸化錫粒子が膜上に定着し難くなるため、5 乃至500nm が好ましいものである。

【0038】また、前記酸化アンチセンをドーパントと する酸化錫粒子の粒径は、100nmを超えると下地層の酸 30 化物膜あるいは混合酸化物膜上に定着し難くなるため、 100mm 以下が好ましい。

【0039】本発明において使用するフルオロアルキル シランの種類としては、例えばCF3 CH2 CH2 Si (OMe)3 CF3 CH2 CH2 SiCl3 CF3 (CF<sub>2</sub>)<sub>5</sub> CH<sub>2</sub> CH<sub>2</sub> Si (OMe)<sub>3</sub> CF 3 (CF2) 5 CH2 CH2 Si (OMe) Cl3 C F3 (CF2)7 CH2 CH2 Si (OMe)3 CF 3 (CF2 ) 7 CH2 CH2 SiCl3 , CF3 (CF 2)7 CH2 CH2 SiMe (OMe)2 CF3 (C 40 F2 ) 7 CH2 CH2 SiMe (C1) 2 などを挙げる ことができる。

【0040】また、本発明において使用する酸化アンチ モンをドーパントとする酸化錫としては、酸化錫のHOMO (Highest Occupied Molecular Orbital) & LUMO (Lowest Unoccupied Molecular Orbital) 間のバンドエネルギー ギャップ間に酸化アンチモンの不純物HOMOレベルを形成 し、半導体性を発現するもので、フルオロアルキルシラ ンの光劣化を抑制するため用いる。酸化錫はcassiterit e(錫石) の結晶構造を有しており、その結晶格子の中に 50 行えず、フルオロアルキルシランの基板への結合量が少

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酸化アンチモンが侵入型固溶体として存在していると考 えられ、酸化アンチモンが酸化錫の結晶格子中にドープ されることにより酸化錫の部分還元がおこり(SnO2-x ・ Sb2O3+x )酸化錫のLUMOレベルに余剰電子が供給され電 子導電性が発現するものである。具体的には例えば商品 名『-1 (三菱マテリアル(株))や商品名エルコム(触 媒化成工業(株))がある。また、予めシリコン化合物 と酸化アンチモンをドーパントとする酸化錫粒子を含ん だゾルとしては、例えば商品名エルコムCT(触媒化成

【0041】またさらに、前記したシリコン化合物とし ては、例えばテトラメトキシシラン〔Si(OM e) 4 ]、テトラエトキシシランSi(OEt) 4 ]、 メチルトリエトキシシラン (MeSi (OEt)3)、 メチルトリメトキシシランMeSi (OMe)3 〕を原 料とした加水分解物が好ましいものである。

【0042】また、前記した有機溶媒としては、メタノ ール、エタノール、プロパノール、ブタノール等のアル コール類、酢酸メチルエステル、酢酸エチルエステル等 のエステル類、ジエチルエーテル等のエーテル類、アセ トン、メチルエチルケトン等のケトン類、エチルセロソ ルブ等が一種または二種以上混合して用いることができ る。

【0043】また、前記した酸はフルオロアルキルシラ ンを加水分解する際の触媒として働くが、硫酸、硝酸、 塩酸、燐酸、芳香族スルホン酸、脂肪族スルホン酸など を用いることができる。特に好ましいのは、硫酸、硝 酸、塩酸などの強酸である。

【0044】また、前記したこれらの混合溶液中のフル オロアルキルシラン量としては、0.1 重量%未満では充 分な飛水性が得られず、20重量%を超えると酸化アンチ モンをドーパントとする酸化錫微粒子に対しフルオロア ルキルシラン量が相対的に多くなり、酸化アンチモンを ドーパントとする酸化錫微粒子の添加効果が発現し難く なるため0.1 ~20重量%である。

【0045】さらに、前記した酸化アンチモンをドーパ ントとする酸化錫微粒子は、焼水性ガラスの焼水性能の 耐久性を向上せしめる効果があり、その量とてしては、 0.04重量%未満では添加効果がなく、2重量%を超える と初期の飛水性を低下させるため、0.1 乃至2重量%で ある。

【0046】さらにまた、前記したシリコン化合物は、 ことに酸化アンチモンをドーパントとする酸化錫微粒子 を酸化物膜表面に安定して固定させるために必要であ り、その量としては、0.03重量%未満では添加効果がな く、2重量%を超えると初期の廃水性を低下させるた め、0.1 乃至2重量%である。

【0047】また、前記した水の添加量は、0.005 重量 %未満ではフルオロアルキルシランの加水分解を充分に

なくなるため、飛水廃油性能が充分に得られない。また 15重量%を超えるとフルオロアルキルシラン同士やシリコン化合物との間で重縮合が進み易く凝集が生じるため、充分な飛水廃油性能が得られなかったり、液の保存安定性が低下したりするため、0.005~15重量%である

【0048】さらにまた、酸の添加量は、フルオロアルキルシラン1mol に対して5×10<sup>-4</sup>mol 未満では添加効果がなく、2×10<sup>-2</sup>mol を超えると処理剤中でフルオロアルキルシラン同士やシリコン化合物との重縮合が促進 10されるため、充分な税水税油性能が得られなかったり、液の保存安定性が低下したりするため、フルオロアルキルシラン1mol に対して5×10<sup>-4</sup>mol ~2×10<sup>-2</sup>mol である

【0049】またさらに、前記混合溶液からなる税水挽油液を酸化物膜あるいは混合酸化物膜上に塗布し乾燥することによって、密着性、耐候性に優れた税水焼油性が得られ、乾燥焼き付ける温度としては、100℃未満でも400℃を超える温度でも税水性ガラスの税水性能の耐久性が向上しないため、100乃至400℃で焼き付けることで税水性能のさらに優れた耐久性能を得ることができる。好ましくは150乃至350℃、より好ましくは200~300℃程度であって、より安定かつ確実にその性能を発現するものとなるものである。なお保持時間としては20~流流へ40分間程度である。

【0050】さらにまた、塗布方法としては、浸せき引き上げ法、スプレー法、フローコート法あるいはスピンコート法、あるいは溶液を含ませた刷毛や綿布等で塗布するなど、既知の塗布手段が適宜採用し得るものである。

# [0051]

【作用】前述したように、本発明によれば、ガラス基板 の表面に、表面処理することなく成膜した状態で、すな わち550 ~650 ℃で焼成後においてもそのままの形状を 保持するマイクロピット状表層、凹凸状表層、凸状表層 のうち少なくとも1種でなる酸化物膜あるいは混合酸化 物膜、すなわち膜厚が10~300nmであって、マイクロビ ット状、凹凸状、凸状がR max = 5~60nm、R a = 2~ 20nm、R z = 5~55nm、S m = 5~700nmであるか、ま たは/およびスキューネスが0乃至>0、クリトシスが 40 3乃至>3である当該膜が下地層としてあり、さらにそ の上に飛水層がが各々特定した量で配分した少なくとも フルオロアルキルシランと酸化アンチモンをドーパント とする酸化錫とシリコン化合物と水および有機溶媒から なる混合溶液に、酸をフルオロアルキルシランに対し特 定量添加した挽水挽油液を塗布成膜することでなる挽水 性ガラスおよびその製造方法とすることにより、適度に 尖った円錐状の山を主とする無平坦状に乱立多在する特 異なマイクロピット状、凹凸状、凸状をなす表層であっ て、保存安定性に優れた挠水挠油液を用いることがで

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き、マイクロピット状、凹凸状、凸状にのめり込むよう にして充分な量の該税水税油液を保持し得、均質かつ均 一に安定かつ確実な成膜処理をすることができることと なる。

【0052】上述したように、ことに特定した特異な下地層ならびに特定した疣水焼油液による疣水層の組み合わせたことにより、初期接触角が115~110°、スーパーJV2000時間後の接触角が104~100°、ワイパー揺動10万回後の接触角が101~99°である等、これら3者ともクリアーできることとなり、下地層はもちろん飛水層も含む膜全体の強度アップに繋がり、疣水層自身の優れた疣水性能、密着性を有し硬い、ならびにことに疣水性能の優れた耐候性、耐久性を示すものとなって、車輌用、船舶用、航空機用あるいは建築用の窓材または各種製品、さらにはミラーガラス等に格段に有用な疣水性ガラスとその製造方法となる。

## [0053]

【実施例】以下、実施例により本発明を具体的に説明する。ただし本発明は係る実施例に限定されるものではない。

## 【0054】実施例1

大きさ約100mm ×100mm 、厚さ約2mmのクリア・フロートガラス基板を中性洗剤、水すすぎ、アルコールで順次 洗浄し、乾燥した後、アセトンで払拭し被膜用基板とした。

【0055】シリカゾル(平均分子量:約3000、固形分 漁度:約30重量%)約20.0g、シリカゾル(平均分子 量:約100000、固形分漁度:約6重量%)約28.6gをビ ーカーに入れ、低平均分子量の固形分/高平均分子量の 30 固形分を約3.5 のmol 比とし、イソプロビルアルコール 約50gならびに1ーブタノール約100 gで希釈し、約15 時間攪拌してコーテイング溶液を得た。

【0056】ついで、該溶液をディッピング法により前 記ガラス基板表面に、約23℃、相対湿度約50%の環境で 成膜し、約270 ℃で約10分間加熱してゲル膜を形成し、 膜厚約150nm 、さらに約600 ℃、約3分間程度焼成後、 膜厚が約100m 程度であった。表層の表面形状を走査型 プローブ顕微鏡NV2000の AFM [原子間顕微鏡、スキャン ライン: 256 本、スキャンサイズ:4,000nm、オリンパス 光学工業(株)〕で測定したところ、表1に示すよう  $C = R_{\text{max}} = 23.9 \text{nm}$   $R_{\text{a}} = 6.2 \text{nm}$   $R_{\text{z}} = 22.1 \text{nm}$ S a =621nm 、その径は約672nm 以内、平均径約50nm程 度であるマイクロピット状乃至凹凸状の表層を呈する酸 化物膜を得た。また、当該膜は表1に〇印で示したよう にスキューネス (Rsk )がO乃至>O、クリトシス (Rk r ) が3乃至>3からRsk が0乃至0に近い>0、Rkr が3乃至3に近い>3となり所期の下地層膜であった。 【0057】さらについで、該マイクロピット状乃至凹 凸状の表層薄膜上に、予め下記の配合で液を混合し、約 50 30分間撹拌して挽水挽油液として調製してあった混合溶 液を塗布した。なお、本実施例による税水税油液の組成 比を表2に示す。

【0058】( ( 雅水雅油液の配合) シリカゾルのエタノ ール溶液1g(平均分子量:約3000、固形分濃度:1wt %)、T-1 (商品名:三菱マテリアル (株) 製、酸化ア ンチモンをドーパントとする酸化錫微粉末(粒径:約20 nm) ] 0.01g、イソプロピルアルコール5.72g、ヘプタ デカトリデシルフルオロアルキルシラン (CF2)7CH2 CltzSi (OMe)3 ] 1 g、pH 1.5硝酸水溶液0.2 g、水0.2 g、合計8.13g。

【0059】その後約250℃で約30分間乾燥することに より、挽水性ガラスを得た。得られた挽水性ガラスにつ いて、下記の試験を行った。

(税水性試験) 大気中(約25℃) での水に対する接触角 を測定。

【0060】(耐候性試験)スーパーUVにより評価。 条件:60ml/cm² で2000時間後の接触角を測定。

(耐摩耗性試験) 自動車用ワイパーによる摺動耐久性に より評価。

【0061】条件:上水を滴下しながら、105 gの荷重 20 をかけて10万回(往復を1回とする)の摺動を行い、接

その結果は、表2に示すように、初期接触角が112° 耐候性試験後でも接触角が103°となって充分優れ、耐 摩耗性試験後でも接触角が100 \* と充分優れるものであ った。調製した廃水廃油処理液は約1ヵ月後においても 凝集するような兆候もなく、酸化錫粒子が良く分散した 状態で充分安定した液であった。

## 【0062】実施例2

実施例1と同様なガラス基板に、実施例1の低平均分子 30 1.5硝酸水溶液0.2 g、水0.2 g、合計5.0 g。 量のシリカゾル約30gと高平均分子量のシリカゾル約2 3.1gをビーカーに入れ、低平均分子量/高平均分子量 の固形分を約6.5 のmol 比とし、他は実施例1と同様と した。得られた酸化物膜は、表1に示すように、膜厚が 約50nm、R max = 12.2nm、R a = 3.4nm 、R z = 11.0n ■、S ■ =約423nm であり、その凹凸の径は約510nm 以 内、平均径約100nm 程度であるマイクロピット状を含む 凹凸状表層を有するものとなった。また、当該膜は表1 に〇印で示したようにRsk が0乃至>0、Rkr が3乃至 >3からRsk が0乃至0に近い>0、Rkr が3乃至3に 40 近い>3となり所期の下地層膜であった。

【0063】さらに次いで、下記の配合で飛水廃油液を 調製し、実施例1と同様に、該マイクロピット状を含む 凹凸状表層薄膜上に揺水揺油処理を行った。本実施例の 税水税油液の組成比および評価結果は表2に示す。

【0064】すなわち、挽水挽油液の配合は、シリカゾ ルのエタノール溶液100 g (平均分子量: 約3000、固形 分濃度: 1 wt%)、T-1 (商品名:三菱マテリアル

(株) 製〕1g、イソプロピルアルコール888g、ヘプ タデカトリデシルフルオロアルキルシラン1g、pH 1.5 50 調製し、実施例1と同様に、該マイクロビット状乃至凸

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硝酸水溶液0.2 g、水9.8 g、合計 1000.0 g。 【0065】得られた飛水性ガラスは、初期接触角が11 2°、耐候性試験後でも接触角が102°となって充分優 れ、耐摩耗性試験後でも接触角が100°と充分優れるも のであった。調製した税水税油処理液は充分安定した液 であって、実施例1と同様となり、所期の飛水性能を発 揮するものであった。

#### 【0066】実施例3

実施例1と同様なガラス基板に、実施例1の低平均分子 10 量のシリカゾル約40gと高平均分子量のシリカゾル約1 8.2gをビーカーに入れ、低平均分子量/高平均分子量 の固形分を約11のmol 比とし、他は実施例1と同様とし た。得られた酸化物膜は、表1に示すように、膜厚が約 60nm, R aax = 11.1nm, R a = 2nm, R z = 10.0nm, S ■ =約358 を有するマイクロピット状を含む凸状であ り、マイクロビット状を含む凸状の径は約380~500mm を有するものとなった。 また、 当該膜は表 1 に〇印で示 したようにRsk がO乃至>O、Rkr が3乃至>3からRs k が0乃至0に近い>0、Rkr が3乃至3に近い>3と なり所期のめざす下地層膜であった。

【0067】さらに次いで、下記の配合で廃水廃油液を 調製し、実施例1と同様に、該マイクロピット状を含む 凸状表層薄膜上に飛水飛油処理を行った。本実施例の飛 水焼油液の組成比および評価結果は表2に示す。

【0068】すなわち、飛水飛油液の配合は、シリカゾ ルのエタノール溶液(平均分子量:約3000、固形分濃 度: 1wt%) 1g、『-1 (商品名:三菱マテリアル (株) 製〕0.01g、イソプロピルアルコール2.59g、ヘ プタデカトリデシルフルオロアルキルシラン1g、pH

【0069】得られた脱水性ガラスは、初期接触角が11 4 °、耐候性試験後でも接触角が103 °となって充分優 れ、耐摩耗性試験後でも接触角が101 °と充分優れるも のであった。調製した撥水猊油処理液は充分安定した液 であって、実施例1と同様となり、所期の優れる飛水性 能を発揮するものであった。

#### 【0070】実施例4

実施例1と同様なガラス基板に、実施例1において使用 したコーティング溶液を使用し、成膜時の相対湿度を約 35%とし、その他は実施例1と同様にした。得られた酸 化物膜は、表1に示すように、膜厚が約80mm、R max = 20.2nm、R a =4.3nm 、R z =18.3nm、S m =約452nm の凸状を有し、表面に径が約10~20mmのマイクロピット を有するマイクロビット状乃至凸状表層となった。ま た、当該膜は表1に〇印で示したようにRsk が0乃至> O、Rkr が3乃至>3からRsk が0乃至0に近い>0、 Rkr が3乃至3に近い>3となり所期のめざす下地層膜 であった。

【0071】さらに次いで、下記の配合で挽水挽油液を

状表層薄膜上に飛水飛油処理を行った。本実施例の飛水 飛油液の組成比および評価結果は表2に示す。

【0072】すなわち、挽水挽油液の配合は、シリカゾルのエタノール溶液(平均分子量:約3000、固形分濃度:1 wt%)1g、T-1〔商品名:三菱マテリアル(株)製〕0.01g、イソプロピルアルコール22.59g、ヘプタデカトリデシルフルオロアルキルシラン1g、叶1.5硝酸水溶液0.2g、木0.2g、合計8.13g。

【0073】得られた飛水性ガラスは、初期接触角が114、耐候性試験後でも接触角が104°となって充分優 10れ、耐摩耗性試験後でも接触角が100°と充分優れるものであった。調製した飛水焼油処理液は充分安定した液であって、実施例1と同様となり、所期の優れる飛水性能を発揮するものであった。

#### 【0074】実施例5

実施例1と同様なガラス基板を用い、テトラエトキシシラン [Si (OCalla)4: TEOS] を16g、エタノール (EtO lt) を8.5 g、水 (予めHCI でpH4に調整) を5.5 gそれぞれ秤り取り、約80℃で約20時間加熱環流を行い、ゾル溶液Aとした。該ブル溶液Aの重量平均分子量 (Mu.ポリスチレン換算値) を測定したところ、約40,000であった。

【0075】メチルトリメトキシシラン〔ChaSi (OC ha)a: MTMS〕を36.6g、イソプロビルアルコール(iPA)を約28.9gおよび純水(pH7)を14.5g秤り取り、約70℃で約5時間加熱還流を行い、ゾル溶液Bとした。該ゾル溶液Bの平均分子量を測定したところ、約2,000 であった。

【0076】上記溶液Aと溶液Bを混合し、約350 gの iPA で希釈し、室温で約10時間攪拌し、溶液Aと溶液B の固形分 (SiOzとして換算) のモル比が1:3.5 である コーテイング溶液を得、ディッピング法により、前記ガ ラス基板表面に、約23℃、相対温度約50%の環境で被膜 し、約100 ℃で約30分間加熱し、膜厚が約150mm のSiO2 のゲル膜を得た。さらに約600 ℃、約3分間程度焼成 後、膜厚が約90mmであり、前記顕微鏡と約2万倍の倍率 で表面状態を観察したところ、表1に示すように、R max =35.5nm、R a =7.8nm 、R x =33.1nm、S m =約 657mm 以内の凸状等を有し、約10~50mmの径を有するマ イクロピット状乃至凹凸状表層をなしていた。また、当 40 該膜は表1に○印で示したようにRsk が0乃至>0、Rk r が3乃至>3からRsk が0乃至0に近い>0、Rkr が 3乃至3に近い>3となり所期のめざす下地層膜であっ た。

【0077】さらに次いで、下記の配合で焼水焼油液を 調製し、実施例1と同様に、該マイクロピット状乃至凹 凸状表層薄膜上に飛水焼油処理を行った。本実施例の焼 水焼油液の組成比および評価結果は表2に示す。

【0078】すなわち、 挽水挽油液の配合は、 シリカゾ ルのエタノール溶液 (平均分子量: 約3000、 固形分濃 16

度:1 wt%)1g、T-1 [商品名:三菱マテリアル (株)製]0.16g、イソプロピルアルコール5.44g、ヘプタデカトリデシルフルオロアルキルシラン1g、pl 1.5硝酸水溶液0.2g、水0.2g、合計8.00g。【0079】得られた洗水性ガラスは、初期接触角が112。、耐候性試験後でも接触角が104。となって充分優れ、耐摩耗性試験後でも接触角が101。と充分優れるものであった。調製した洗水焼油処理液は充分安定した液であって、実施例1と同様となり、所期の優れる洗水性能を発揮するものであった。

#### 【0080】実施例6

実施例1と同様なガラス基板に、テトラプロポキシドチ タン (Ti (OiPr)4 ) 2.8 g、iPA 46.6gならびに水 (pH 2) 0.6 gを秤り取り、室温で約30分間攪拌を行い、溶 液Cとした。実施例5と同様に溶液Aと溶液Bを混合し た後、該溶液Cを加え、その後iPA 300 gをさらに加え てコーテイング溶液を調製した。該コーテイング溶液に おける溶液Aと溶液Bとの固形分(SiOzとして換算)と 溶液Cの固形分(TiOzとして換算)とのモル比は1:3. 5:0.45である。実施例5と同様にして、膜厚約70nmの SiOz·TiOz混合薄膜を得た。表面状態を観察したとこ ろ、表1に示すように、R max =15.8nm、R a =4.7 n ■、R z =14.4nm、S m =約488nm の凹凸乃至凸状を有 し、約10~50nmの径を有するマイクロピット状を含む凹 凸乃至凸状表層をなしていた。また、当該膜は表1に○ 印で示したようにRsk が0乃至>0、Rkr が3乃至>3 からRsk が0乃至0に近い>0、Rkr が3乃至3に近い >3となり所期のめざす下地層膜であった。

【0081】さらに次いで、下記の配合で雅水雅油液を 調製し、実施例1と同様に、該マイクロピット状を含む 凹凸乃至凸状表層薄膜上に飛水雅油処理を行った。本実 施例の飛水雅油液の組成比および評価結果は表2に示 す。

【0082】すなわち、税水税油液の配合は、シリカゾルのエタノール溶液(平均分子量:約3000、固形分濃度:1wt%)2g、T-1〔商品名:三菱マテリアル(株)製〕0.01g、イソプロピルアルコール46.59g、ヘプタデカトリデシルフルオロアルキルシラン1g、60%硝酸水溶液0.2g、水0.2g、合計50.0g。

【0083】得られた飛水性ガラスは、初期接触角が111、耐候性試験後でも接触角が100°となって充分優れ、耐摩耗性試験後でも接触角が100°と充分優れるものであった。調製した飛水焼油処理液は充分安定した液であって、実施例1と同様となり、所期の優れる飛水性能を発揮するものであった。

## 【0084】実施例7

溶液A、B、Cそれぞれの固形分のモル比が1:11:1. 2となるようにコーテイング溶液を調製する以外、実施 例6と同様にして膜厚約50nmの前記下地層薄膜を得た。

50 表面状態を観察したところ、表1に示すように、R max

=17.8nm、R a=5.3nm 、R z =16.2nm、S m =約414nm の凹凸乃至凸状を有し、約10~50mmの径を有するマイ クロピット状を含む凹凸状乃至凸状表層をなしていた。 また、当該膜は表1に〇印で示したようにRsk が0乃至 >0、Rkr が3乃至>3からRskが0乃至0に近い> 0、Rkr が3乃至3に近い>3となり所期のめざす下地 層膜であった。

【0085】さらに次いで、下記の配合で挽水飛油液を 調製し、実施例1と同様に、該マイクロピット状を含む 凹凸状乃至凸状表層薄膜上に挽水脱油処理を行った。本 10 度:1 wt%) 0.75g、『-1〔商品名:三菱マテリアル 実施例の飛水飛油液の組成比および評価結果は表2に示 す。

ルのエタノール溶液(平均分子量:約3000、固形分濃 度:1wt%)1g、T-1(商品名:三菱マテリアル (株) 製) 0.01g、イソプロピルアルコール3.21g、ヘ プタデカトリデシルフルオロアルキルシラン1g、叶 1.5硝酸水溶液0.2 g、水1g、合計6.42g。

【0087】得られた飛水性ガラスは、初期接触角が11 4 \* 、耐候性試験後でも接触角が104 \* となって充分優 20 れ、耐摩耗性試験後でも接触角が100°と充分優れるも のであった。調製した飛水飛油処理液は充分安定した液 であって、実施例1と同様となり、所期の優れる飛水性 能を発揮するものであった。

# 【0088】実施例8

たこと以外は、実施例1と同様にした。

【0089】すなわち、飛水쁐油液の配合は、シリカゾ ルのエタノール溶液(平均分子量:約3000、固形分濃 度: 1 wt%) 1g、『-1 (商品名: 三菱マテリアル (株) 製] 0.01g、イソプロピルアルコール5.59g、ヘ プタデカトリデシルフルオロアルキルシラン1g、叶 2.1硝酸水溶液0.11g、水0.29g、合計8.00g。

【0090】得られた脱水性ガラスは、表2に示すよう に、初期接触角が113°、耐候性試験後でも接触角が10 2°となって充分優れ、耐摩耗性試験後でも接触角が99 ・と充分優れるものであった。調製した稅水稅油処理液 は充分安定した液であって、実施例1と同様となり、所 期の優れる税水性能を発揮するものであった。

## 【0091】実施例9

たこと以外は、実施例3と同様にした。

【0092】すなわち、挽水挽油液の配合は、シリカゾ ルのエタノール溶液 (平均分子量:約3000、固形分濃 度: 1wt%) 1g、T-1 (商品名: 三菱マテリアル (株) 製) 0.01g、イソプロピルアルコール5.59g、ヘ プタデカトリデシルフルオロアルキルシラン1g、H 1.1硝酸水溶液0.4 g、水0g、合計8.00g。

【0093】得られた脱水性ガラスは、表2に示すよう に、初期接触角が115 。、耐候性試験後でも接触角が10 50 液は充分安定した液であって、実施例1と同様となり、

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2°となって充分優れ、耐摩耗性試験後でも接触角が10 0°と充分優れるものであった。調製した飛水飛油処理 液は充分安定した液であって、実施例1と同様となり、 所期の優れる飛水性能を発揮するものであった。

#### 【0094】実施例10

たこと以外は、実施例2と同様にした。

【0095】すなわち、飛水飛油液の配合は、シリカゾ ルのエタノール溶液(平均分子量:約3000、固形分濃 (株) 製) 0.01g、イソプロピルアルコール22.84 g、 ヘプタデカトリデシルフルオロアルキルシラン1g、pH 1.5硝酸水溶液0.2 g、水0.2 g、合計24.0g。

【0096】得られた撥水性ガラスは、表2に示すよう に、初期接触角が112 °、耐候性試験後でも接触角が10 4°となって充分優れ、耐摩耗性試験後でも接触角が10 0 ・ と充分優れるものであった。調製した飛水挽油処理 液は充分安定した液であって、実施例1と同様となり、 所期の優れる飛水性能を発揮するものであった。

## 【0097】実施例11

実施例4において、攪水攪油液の配合を次のように変え たこと以外は、実施例4と同様にした。

【0098】すなわち、飛水溌油液の配合は、シリカゾ ルのエタノール溶液(平均分子量:約3000、固形分濃 度: 1 wt%) 1.6 g、T-1 (商品名: 三菱マテリアル (株) 製) 0.01g、イソプロピルアルコール4.99g、ヘ プタデカトリデシルフルオロアルキルシラン1g、pH 1.5硝酸水溶液0.2 g、水0.2 g、合計8.00g。

【0099】得られた飛水性ガラスは、表2に示すよう 30 に、初期接触角が111 °、耐候性試験後でも接触角が10 3 ・となって充分優れ、耐摩耗性試験後でも接触角が10 0°と充分優れるものであった。調製した飛水飛油処理 液は充分安定した液であって、実施例1と同様となり、 所期の優れる飛水性能を発揮するものであった。

# 【0100】実施例12

たこと以外は、実施例1と同様にした。

【0101】すなわち、飛水飛油液の配合は、酸化アン チモンをドーバントとする酸化錫微粒子(粒径:5nm) 40 のゾル液〔固形分濃度2.5 xt%,シリコン化合物として 1.11wt%, 酸化アンチモンをドーバントとする酸化錫と して1.39xt%のもの、触媒化成(株)製〕1g、イソプ ロピルアルコール5g、ヘプタデカトリデシルフルオロ アルキルシラン1g、pl 2.5硝酸水溶液0.4 g、水0 g、合計7.4 g。

【0102】得られた脱水性ガラスは、表2に示すよう に、初期接触角が113 °、耐候性試験後でも接触角が10 2°となって充分優れ、耐摩耗性試験後でも接触角が10 0°と充分優れるものであった。調製した飛水焼油処理 19

所期の優れる飛水性能を発揮するものであった。 【0103】実施例13

たこと以外は、実施例2と同様にした。

【0104】すなわち、挽水飛油液の配合は、酸化アン チモンをドーバントとする酸化錫微粒子(粒径:5mm) のゾル液 [固形分濃度2.5 xt%, シリコン化合物として 1.11wt%, 酸化アンチモンをドーパントとする酸化錫と して1.39xt%のもの、触媒化成(株)製]1g、イソプ ロピルアルコール25g、ヘアタデカトリデシルフルオロ\*10 【表1】

\*アルキルシラン1g、pll 2.5硝酸水溶液0.4 g、水0 g、合計27.4g。

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【0105】得られた猊水性ガラスは、表2に示すよう に、初期接触角が111 °、耐候性試験後でも接触角が10 1 となって充分優れ、耐摩耗性試験後でも接触角が99 \*と充分優れるものであった。調製した稅水稅油処理液 は充分安定した液であって、実施例1と同様となり、所 期の優れる飛水性能を発揮するものであった。

[0106]

|      |   |       |                      |              | F          | 油 眉        |            | •                            |      |
|------|---|-------|----------------------|--------------|------------|------------|------------|------------------------------|------|
|      | 医温波<br>S:SiO <sub>2</sub><br>T:TiO <sub>2</sub> | (0 m) | 表層形状<br>性マイクロ<br>ピット | Rmux<br>(nm) | Ra<br>(nm) | Rz<br>(nm) | Sm<br>(nm) | Rsk&Rkr<br>(0~>0,0<br>~>3=0) | (nm) |
| 実施例1 | S   | 100   | M. 国的                | 23. 9        | 6. 2       | 22. 1      | 621        | 0                            | 5 0  |
| 2    | S   | 50    | W. END               | 12. 2        | 3. 4       | 11.0       | 423        | 0                            | 400  |
| 8    | S   | 60    | м, д                 | 11. 1        | 2. 0       | 10.0       | 358        | 0                            | 400  |
| 4    | S   | 8 0   | W 🖫                  | 20. 2        | 4. 3       | 18. 3      | 452        | 0                            | 3 0  |
| 5    | S   | 90    | M' 🖫                 | 35. 5        | 7. 8       | 33. 1      | 657        | 0                            | 3 0  |
| 6    | S·T   | 70    | M' 🙀                 | 15. 8        | 4. 7       | 14. 4      | 488        | 0                            | 3 0  |
| 7    | S·T   | 50    | 九四公、八                | 1.7. 8       | 5. 3       | 16. 2      | 414        | 0                            | 3 0  |
| 8    | S   | 100   | 米區凸                  | 23. 9        | 6. 2       | 2 2. 1     | 672        | 0                            | 5 0  |
| 9    | S   | 50    | M. A                 | 11. 1        | 2. 0       | 10.0       | 3 5 8      | 0                            | 400  |
| 10   | S   | 5 0   | 14、国内                | 12. 2        | 3. 4       | 11.0       | 510        | 0                            | 400  |
| 11   | S   | 8 0   | W. D                 | 20. 2        | 4. 3       | 18.3       | 452        | 0                            | 3 0  |
| 12   | S   | 100   | M. 图凸                | 23. 9        | 6. 2       | 2 2. 1     | 672        | 0                            | 5 0  |
| 13   | S   | · 5 0 | M. 图型                | 12. 2        | 3. 4       | 11.0       | 423        | 0                            | 400  |

[0107]

※ ※【表2】

|      |        | 整水量站    | 大の配合 (重)                 | 200                      |             | (m o 1)                |                  | 評価                    |                        |
|------|--------|---------|--------------------------|--------------------------|-------------|------------------------|------------------|-----------------------|------------------------|
|      | 水      | 有概溶媒    | フルオロア<br>ルキルシラ<br>ン(FAS) | 後化線 (酸<br>化アンチモ<br>ンドープ) | シリコン化<br>合物 | PAS1モルに対<br>する酸のモル数    | 初期接<br>触角<br>(*) | 耐候性試験<br>後の接触角<br>(゜) | 副学年性試<br>験後の接触<br>角(*) |
| 実施例1 | 4. 92  | 82.54   | 12.3                     | 0. 12                    | 0. 12       | 3. 70×10 <sup>-3</sup> | 112              | 103                   | 100                    |
| 2    | 1      | 98.7    | 0. 1                     | 0. 1                     | 0. 1        | 3. 70×10 <sup>-3</sup> | 112              | 102                   | 100                    |
| 3    | 8      | 71.6    | 2 0                      | 0. 2                     | 0. 2        | 3. 70×10-3             | 114              | 103                   | 101                    |
| 4    | 1. 6   | 94. 32  | 4                        | 0. 04                    | 0. 04       | 3. 70×10 <sup>-3</sup> | 114              | 104                   | 100                    |
| 5    | 5      | 80.38   | 12.5                     | 2                        | 0. 12       | 3. 70×10-*             | 112              | 104                   | 101                    |
| 6    | 0. 005 | 86. 245 | 12.5                     | 0. 125                   | 0. 125      | 5. 60×10-*             | 111              | 100                   | 100                    |
| 7    | 1 5    | 72. 25  | 12.5                     | 0. 125                   | 0. 125      | 3. 70×10 <sup>-3</sup> | 114              | 104                   | 100                    |
| 8    | 5      | 82. 25  | 1 2. 5                   | 0. 125                   | 0. 125      | 5. 10×10 <sup>-4</sup> | 113              | 102                   | 9 9                    |
| 9    | 5      | 82. 25  | 12.5                     | 0. 125                   | 0. 125      | 1. 90×10 <sup>-1</sup> | 1.1 5            | 102                   | 100                    |
| 10   | 1. 6   | 94. 33  | 4                        | 0.04                     | 0. 03       | 1. 90×10 <sup>-3</sup> | 112              | 104                   | 100                    |
| 11   | 5      | 80.38   | 12.5                     | 0.12                     | 2           | 1. 90×10 <sup>-3</sup> | 111              | 103                   | 100                    |
| 12   | 5. 4   | 80.75   | 13. 51                   | 0. 19                    | 0. 15       | 7. 40×10 <sup>-4</sup> | 113              | 102                   | 100                    |
| 13   | 1. 46  | 94.8    | 3. 65                    | 0.05                     | 0.04        | 7. 40×10 <sup>-4</sup> | 111              | 101                   | 9 9                    |

【0108】比較例1

★ティング溶液とした。それ以外は実施例1と同様とし

た。得られた下地層膜は、膜厚が約150nm 、表面が平均 シリカゾル (平均分子量:約100000、固形分濃度:約6 重量%)を約200 gをビーカーにはかり、そのままコー★50 径約2nmのマイクロピット状ではあるが平滑面に近い表 層を呈するものを得た。次いで下記の配合で飛水飛油処 理液を調製し、実施例1と同様に下地層上に飛水処理を す。

【0109】すなわち、挽水挽油処理液の配合は、シリ カゾルのエタノール溶液 (平均分子量:約3000、固形分 濃度: 1 wt%) 100 g、₹-1 (商品名: 三菱マテリアル (株) 製〕1g、イソプロピルアルコール889g、ヘブ タデカトリデシルフルオロアルキルシラン0.5 g、pH 1.5硝酸水溶液0.2 g、水9.8 g、合計1000.5g。

【0110】得られた飛水飛油処理ガラスは、初期接触 角が100 ° であるものの、耐候性試験後では接触角が78 ・となって極端に悪く、耐摩耗性試験後でも接触角が72 ・と悪く、下地層が平坦状で上述した各実施例と異な り、前記各実施例から耐摩耗性はもちろん、所期の耐候 性が著しく劣り、優れる飛水性能を有するものであると は到底言えないものであった。

# 【0111】比較例2

比較例1において、 挽水廃油処理液の配合を次のように 変えたこと以外は、比較例1と同様にした。 飛水飛油液 20 の配合比および評価結果は表3に示す。

【0112】すなわち、飛水飛油処理液の配合は、シリ カゾルのエタノール溶液 (平均分子量: 約3000、固形分 濃度: 1 wt%) 1 g、T-1 (商品名:三菱マテリアル (株) 製] 0.01g、イソプロピルアルコール1.59g、ヘ アタデカトリデシルフルオロアルキルシラン1g、叶 1.5硝酸水溶液0.2 g、水0.2 g、合計8.00g。

【0113】得られた飛水焼油処理ガラスは、溶剤量が 少ないために処理中に乾燥し面内をむらなく処理するこ とが困難であった。また初期接触角が113°であるもの30 の、耐候性試験後では接触角が92°となったが、耐摩耗 性試験後でも接触角が78°と悪く、下地層が平坦状で上 述した各実施例と異なり、所期の優れる挽水性能を有す るものであるとは到底言えないものであった。さらに該 **飛水飛油処理液は約3日後には凝集し酸化錫の粒子が沈** 殿し不安定なものであった。

## 【0114】比較例3

変えたこと以外は、比較例1と同様にした。 撥水撥油液 の配合比および評価結果は表3に示す。

【0115】すなわち、挽水挽油処理液の配合は、シリ カゾルのエタノール溶液 (平均分子量:約3000、固形分 濃度: 1wt%) 2g、T-1 (商品名:三菱マテリアル (株) 製] 0.01g、イソプロピルアルコール46.59 g、 ヘプタデカトリデシルフルオロアルキルシラン1g、H 1.5硝酸水溶液0.2 g、水0.2 g、合計50.0g。

【0116】得られた飛水飛油処理ガラスは、初期接触 角が112°であるものの、耐候性試験後では接触角が85 \*となったが、耐摩耗性試験後でも接触角が89\*と悪 く、下地層が平坦状で上述した各実施例と異なり、所期 50 た。さらに該撓水撓油処理液は約1日後には凝集し酸化

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の優れる撥水性能を有するものであるとは到底言えない ものであった。

#### 【0117】比較例4

変えたこと以外は、比較例1と同様にした。 쁐水쁐油液 の配合比および評価結果は表3に示す。

【0118】すなわち、挽水挽油処理液の配合は、シリ カゾルのエタノール溶液(平均分子量:約3000、固形分 濃度: 1 wt%) 1g、『-1 (商品名: 三菱マテリアル (株) 製〕0.2 g、イソプロピルアルコール5.4 g、へ 10 プタデカトリデシルフルオロアルキルシラン1g、pH 1.5硝酸水溶液0.2 g、水0.2 g、合計8.00g。

【0119】得られた飛水飛油処理ガラスは、初期接触 角が100°であるものの、耐候性試験後では接触角が76 ・となり、耐摩耗性試験後でも接触角が75°と悪く、下 地層が平坦状で上述した各実施例と異なり、各実施例に 比しその性能は著しく劣り、所期の優れる飛水性能を有 するものであるとは到底言えないものであった。

# 【0120】比較例5

たこと以外は、実施例2と同様にした。 飛水飛油液の配 合比および評価結果は表3に示す。

【0121】すなわち、飛水飛油処理液の配合は、シリ カゾルのエタノール溶液 (平均分子量:約3000、固形分 濃度:1wt%)10g、T-1 (商品名:三菱マテリアル (株) 製] 0.1 g、イソプロピルアルコール59.9g、ヘ プタデカトリデシルフルオロアルキルシラン10g、60% 硝酸水溶液0.005 g、水0g、合計80.005g。

【0122】得られた飛水飛油処理ガラスは、初期接触 角が99°であるものの、耐候性試験後では接触角が88° となり、耐磨耗性試験後でも接触角が88°と悪く、各実 施例と比較しその性能は著しく劣り、所期の優れる飛水 性能を有するものであるとは到底言えないものであっ た。

# 【0123】比較例6

実施例2において、挽水挽油液の配合を次のように変え たこと以外は、実施例2と同様にした。 雅水雅油液の配 合比および評価結果は表3に示す。

【0124】すなわち、 挽水挽油処理液の配合は、シリ カゾルのエタノール溶液(平均分子量:約3000、固形分 40 濃度: 1wt%) 1g、T-1 (商品名: 三菱マテリアル (株) 製] 0.01g、イソプロピルアルコール2.81g、ヘ プタデカトリデシルフルオロアルキルシラン1g、pH1. 5 硝酸水溶液0.2 g、水4g、合計9.02g。

【0125】得られた飛水飛油処理ガラスは、初期接触 角が112 ° であるものの、耐候性試験後では接触角が95 ・となり、耐摩耗性試験後でも接触角が94。と悪く、各 実施例と比較しその性能は著しく劣り、所期の優れる飛 水性能を有するものであるとは到底言えないものであっ

錫の粒子が沈殿し極めて不安定なものであった。 【0126】比較例7

実施例2において、 挽水挽油液の配合を次のように変え たこと以外は、実施例2と同様にした。 雅水飛油液の配 合比および評価結果は表3に示す。

【0127】すなわち、挽水挽油処理液の配合は、シリ カゾルのエタノール溶液(平均分子量:約3000、固形分 濃度: 1 wt%) 1g、『-1 〔商品名: 三菱マテリアル (株) 製] 0.01g、イソプロピルアルコール5.59g、ヘ アタデカトリデシルフルオロアルキルシラン1g、pH2. 10 合比および評価結果は表3に示す。 1 硝酸水溶液0.05g、水0.35g、合計8.00g。

【0128】得られた搬水飛油処理ガラスは、初期接触 角が100°であるものの、耐候性試験後では接触角が87 \*となり、耐摩耗性試験後でも接触角が90°と悪く、各 実施例と比較しその性能は著しく劣り、所期の優れる税 水性能を有するものであるとは到底言えないものであっ

# 【0129】比較例8

合比および評価結果は表3に示す。

【0130】すなわち、挽水挽油処理液の配合は、シリ カゾルのエタノール溶液(平均分子量:約3000、固形分 濃度: 1 wt%) 1 g、T-1 (商品名:三菱マテリアル (株) 製) 0.01g、イソプロピルアルコール5.59g、ヘ アタデカトリデシルフルオロアルキルシラン1g、H1 硝酸水溶液0.4 g、水0g、合計8.00g。

【0131】得られた飛水飛油処理ガラスは、初期接触 角が110°であるものの、耐候性試験後では接触角が97 となり、耐摩耗性試験後でも接触角が94°と悪く、各 30 実施例と比しその性能は劣るものの割合近いが、所期の 優れる挽水性能を有するものであるとは言えないもので あった。さらに該飛水飛油処理液は約1日後には凝集し 酸化錫の粒子が沈殿し極めて不安定なものであった。

## 【0132】比較例9

実施例2において、 
飛水焼油液の配合を次のように変え たこと以外は、実施例2と同様にした。 挽水焼油液の配 合比および評価結果は表3に示す。

【0133】すなわち、飛水飛油処理液の配合は、シリ カゾルのエタノール溶液(平均分子量:約3000、固形分 40 施例と比較しその性能は劣り、所期の優れる飛水性能を 濃度: 1 wt%) 1g、T-1 (商品名: 三菱マテリアル (株) 製] 0.1 g、イソプロピルアルコール47.5g、ヘ プタデカトリデシルフルオロアルキルシラン1g、pH1.

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5 硝酸水溶液0.2 g、水0.2 g、合計50.0g。

【0134】得られた飛水飛油処理ガラスは、初期接触 角が112 ° であるものの、耐候性試験後では接触角が91 \*となり、耐摩耗性試験後でも接触角が92\*と悪く、各 実施例と比較し耐候性が劣り、所期の優れる飛水性能を 有するものであるとは到底言えないものであった。

# 【0135】比較例10

たこと以外は、実施例2と同様にした。 揺水飛油液の配

【0136】すなわち、 挽水脱油処理液の配合は、シリ カゾルのエタノール溶液(平均分子量:約3000、固形分 溫度: 1 wt%) 2 g、『−1 〔商品名:三菱マテリアル (株) 製] 0.01g、イソプロピルアルコール4.59g、ヘ アタデカトリデシルフルオロアルキルシラン1g、pH1 硝酸水溶液0.2 g、水0.2 g、合計8.00g。

【0137】得られた税水稅油処理ガラスは、初期接触 角が109 ° であるものの、耐候性試験後では接触角が90 \*となり、耐摩耗性試験後の接触角が89\*と悪く、各実 有するものであるとは到底言えないものであった。さら に該 飛水 挽油処理液は約3日後には 凝集し酸化鍋の粒子 が沈殿し不安定なものであった。

#### 【0138】比較例11

比較例1において、実施例1の飛水飛油液の配合を用い たこと以外は、比較例1と同様にした。 撓水飛油液の配 合比および評価結果は表3に示す。

【0139】得られた飛水飛油処理ガラスは、初期接触 角が111 ° であるものの、耐候性試験後では接触角が87 ・となり、耐摩耗性試験後の接触角が90°と悪く、各実 施例と比較しその性能は劣り、所期の優れる税水性能を 有するものであるとは到底言えないものであった。

## 【0140】比較例12

比較例1において、実施例7の飛水飛油液の配合を用い 合比および評価結果は表3に示す。

【0141】得られた飛水挽油処理ガラスは、初期接触 角が113 ° であるものの、耐候性試験後では接触角が92 \*となり、耐摩耗性試験後の接触角が89\*と悪く、各実 有するものであるとは到底言えないものであった。

[0142]

【表3】

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|       |                  | お                 |      |       | 数大物油   | 機水器油液の配合 (重量%)         | (%)                  |        | (Ho1)           |     | 是                    |                        |
|-------|------------------|-------------------|------|-------|--------|------------------------|----------------------|--------|-----------------|-----|----------------------|------------------------|
|       | KAL的版<br>S: SiOs | ボロ<br>ボッンク<br>マンシ | (nm) | *     | 有概容牒   | フルキロア<br>ルキルシラ<br>ソGAS | 限分割<br>会インサル<br>シドーン | かってん   | FAS1キルに対する機のモル教 | はい。 | 職権性は<br>第の統計は<br>(・) | 記載を存在<br>を表の行動<br>か(・) |
| 1000年 | s                | 聚山—W              | 2    | 1     | 98.75  | 0.05                   | 0.1                  | 0.1    | 3. 70×10-1      | 100 | 7.8                  | 7.2                    |
| 2     | S                | M—平衡              | 2    | 10    | 64.5   | 2.5                    | 0.25                 | 0.25   | 3. 70×10-1      | 113 | 3 6                  | 7 8                    |
| က     | S                | M一中海              | 3    | 0.8   | 97.14  | 2                      | 0.02                 | 0.04   | 3. 70×10-1      | 112 | 8.5                  | σ<br>∞                 |
| 7     | s                | 聚士—W              | 2    | 5     | 79.88  | 12.5                   | 2. 5                 | 0.12   | 3. 70×10-3      | 100 | 7 6                  | 7.5                    |
| 2     | S                | M, WIL            | 400  | 0.003 | 87.247 | 12.5                   | 0.125                | 0. 125 | 2. 80×10-       | 8 6 | 80<br>80             | 8 8                    |
| 9     | S                | M, III            | 400  | 2 0   | 67.25  | 12.5                   | 0, 125               | 0. 125 | 3. 70×10.       | 211 | 3 5                  | 9.4                    |
| 7     | S                | M. EP.            | 400  | 5     | 82.25  | 12.5                   | 0.125                | 0. 125 | 2. 30×10-4      | 001 | 8.7                  | 0 6                    |
| 8     | S                | M、 따라             | 400  | 5     | 82.25  | 12.5                   | 0. 125               | 0. 125 | 2. 40×10-F      | 110 | 8.7                  | <b>7</b> 6             |
| თ     | S                | M, With           | 400  | 0.8   | 86.98  | 2                      | 0.2                  | 0.02   | 1. 90×10-1      | 112 | 9.1                  | 9.2                    |
| OT.   | S                | M、 따라             | 400  | 5     | 79.88  | 12.5                   | 0.12                 | 2. 5   | 1. 90×10-3      | 109 | 0.6                  | 68                     |
| 11    | S                | M一和新              | 2    | 4.92  | 82.54  | 12.3                   | .0.12                | 0.12   | 3. 70×10.       | 111 | 8.7                  | 0.5                    |
| 12    | S                | M一年               | 2    | 1.5   | 72.25  | 12.5                   | 0. 125               | 0. 125 | 3. 70×10-1      | 113 | 26                   | 68                     |
|       |                  |                   |      |       |        |                        |                      |        |                 |     |                      |                        |

# [0143]

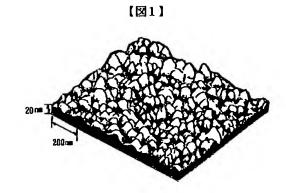
【発明の効果】以上記述したように、本発明の税水性ガラスおよびその製造法によれば、保存安定性に優れた特定した税水税油液でもって、手軽に容易な膜形成手段によって特異な被膜を安価に効率よく得られ、光学特性を損なうことなく、税水性、膜質、密着性、硬さ、耐候性等に長期的に優れるものとなり、ことに格段の税水性能で優れた耐候性、耐摩耗性を示すものとすることがで \*

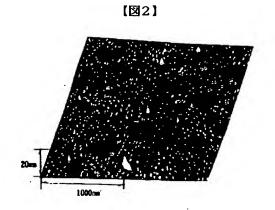
\*き、建築用もしくは自動車用窓材をはじめ、各種ガラス 物品等に好適に採用できる、有用な脱水性ガラスおよび その製造方法を提供するものである。

# 【図面の簡単な説明】

【図1】本発明の一実施例における下地層の表層部分を拡大し簡単な模式図で例示する。

【図2】従来の一例(エッチング処理膜) における下地層の表層部分を拡大し簡単な模式図で例示する。





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## \* NOTICES \*

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## DETAILED DESCRIPTION

[Detailed Description of the Invention] [0001]

[Industrial Application] Water-repellent oil repellency ability of this invention is useful about the water-repellent glass which was excellent in endurance and abrasion resistance from the first, and its manufacture approach to the object for cars, the object for vessels, the object for aircrafts, window glass, a mirror of \*\*\*\*\*\*\*, etc.

[0002]

[Description of the Prior Art] In order to make water-repellent oil repellency give base materials, such as glass and resin, the attempt which carries out spreading membrane formation of the processing agent containing a fluoro alkyl group content compound, dimethylsiloxane, and fluororesin on said base material front face is made. However, only by applying these processing agents, the bonding strength on said front face of a base material was weak, and it was difficult to be fully able to give neither weatherability nor abrasion resistance, but to continue and to maintain water repellence at a long period of time.

[0003] Until now, in order to give water-repellent oil repellency on materials, such as glass, various applications of what used diluents, such as the poly fluoro alkyl group (Rf radical) content silane compound and alcohol, are carried out. For example, they are JP,58-122979,A, JP,58-129082,A, JP,58-172245,A, JP,5-345641,A, etc.

[0004] It is indicated [ that the mixed liquor of a fluoro alkyl group content compound, a silicon compound, alcohol, and an acid is used as a processing agent for the transparence Plastic solid in which water repellence is shown by preparing the low refractive-index layer containing a fluorine compound on it after forming the oxidation tin layer which doped tin oxide and antimony as a high refractive-index dielectric layer on transparence base materials, such as glass, at JP,3-90345,A being indicated, and forming this low refractive-index layer further, for example, etc. and ].

[0005] Moreover, for example, it is 1 micrometer in thickness to which the poly fluoro alkyl group content silane \*\*\*\*\*\*\* becomes JP,58-167448,A from the partial hydrolysis condensate of this compound. The low reflection factor glass made into a low reflection factor and water-repellent oil repellency is indicated without spoiling fluoroscopy nature etc. by forming the following thin films in a glass front face.

[0006] However, in the water-repellent oil-repellent processing using such a conventional processing agent, the bonding strength of the water-repellent oil-repellent radical introduced into a base material front face was weak, in endurance and a weathering test, water repellence deteriorated comparatively for a short time, and there was a trouble that the water-repellent engine performance was not maintainable for a long time.

[0007] Although the glass which covered Teflon was one of those were furthermore excellent in weatherability, there was a trouble that transparency was spoiled immediately that it is easy to get damaged since the film is soft. Moreover, for example, although the water-repellent-finish glass in which the water-repellent coat which consists of both sides of the polymerization object of a fluorine

compound as the polymerization object and the water-repellent component of the organic silicon compound which has siloxane association as an adhesion component was formed on the glass substrate was indicated by JP,60-231442,A, there was a trouble that a front face tends to get damaged since the polymerization object of a water-repellent component has all or composition contained relatively in it. [many]

[0008] Moreover, for example, a metal oxide layer is formed on a plastic plate, and although the surface treatment plastics which carried out the laminating of a metal oxide layer and the compound layer of a fluororesin on it is indicated by JP,3-153859,A, since a substrate is plastics, there are problems, like adhesion is not what can not necessarily be satisfied in it.

[0009] Moreover, for example, although the water-repellent glass which has the hydrophobic layer which consists of a water-repellent particle distributed in the metallic-oxide phase and this metallic-oxide phase on a glass substrate was indicated by JP,5-51238,A, there was a trouble of being easy to get damaged in it, with the configuration which the particle distributed in the film equally.

[0010] Moreover, the metallic-oxide coat was prepared in the glass front face, and further, although giving water repellence by carrying out the ion implantation of the ion of Sn or the element of Sb to the front face was indicated by JP,4-160039,A, there was a trouble that ion oxidized gradually and the water-repellent engine performance could not continue for a long time after that sufficient initial-contact angle is not acquired or impregnation in it, for example.

[0011] moreover, as what prepared the substrate layer and the hydrophobic layer in the base material

front face For example, the metal oxide layer of SiO2 grade is formed in a glass base material front face at JP,2-311332,A. The manufacture approach of water-repellent glass of preparing hydrophobic layers which silanized, such as an alkoxysilane compound and a fluoro alkyl silane compound, is indicated. Furthermore, it is [ that the glass goods which have the durable water repellence front face currently processed by the silica substrate layer and perfluoro-alkyl, and the alkyl silane on the glass base front face are indicated, etc. and 1 in JP,5-238781, A. Especially in these, it was what water-repellent degradation and a minute blemish may be faintly attached in long-term endurance, abrasion resistance. etc. under a harsh environment, and is hard to be referred to as not necessarily enough. [0012] furthermore, as what prepared the concave convex substrate layer in the substrate front face, and prepared the hydrophobic layer on it For example, a metal oxide film is formed in a glass front face at JP,4-124047,A. Prepare irregularity by etching and the water-repellent-finish approach on the front face of glass which coats water-repellent chemicals, such as fluorine silicon which has the poly fluoro alkyl group on it, is indicated. Further again to JP,6-116430,A The inorganic hard film of the SiO(plasma electrodischarge treatment)2 grade in which minute irregularity (granularity is 0.01 - 0.3 mum) was formed on plastic film, It is [ that the water-repellent oil repellency film which consists of a chemisorption monomolecular film containing the fluorine besides made to form through siloxane association is indicated, etc. and ]. It was what is hard to be called what it cannot maintain [in / unlike a thing expected in the shape of toothing / as for all, the irregularity processing is / these / complicated, and / maintenance of endurance long-term / of the water repellence under a harsh environment /

[Problem(s) to be Solved by the Invention] This invention solves the above-mentioned conventional trouble, and the purpose is excellent in adhesion and weatherability, and, moreover, is especially more to offer the water-repellent glass which can maintain hard long-term endurance, abrasion resistance, etc. of the water-repellent engine performance under a harsh environment, and its manufacture approach by [ of the specified water-repellent oil-repellent liquid excellent in the substrate layer and preservation stability of a unique configuration by unique formation ] carrying out a combination laminating. [0014]

moreover especially more, abrasion resistance, etc. ] enough, but water-repellent degradation tended to take place, and a minute blemish may be attached faintly, and is not necessarily satisfied enough.

[Means for Solving the Problem] This invention is made in view of the trouble which the former requires. At least 0.1 - 20 % of the weight of fluoro alkyl silanes, 0.04 - 2 % of the weight of particles of the tin oxide which makes antimony oxide a dopant, 0.03 - 2 % of the weight of silicon compounds, and

[0013]

water to the mixed solution which consists of 0.005 - 15 % of the weight, and an organic solvent It is fluoro alkyl silane 1 mol about an acid. It receives and is - 5x10 to 4 mol 2x10 to 2 mol. The specific water-repellent oil-repellent liquid added so that it might become The coat of an oxide solution or the mixed oxide solution is carried out, and it also sets after baking by 550 - 650 \*\*. As it is The above-mentioned purpose can be attained by applying on the substrate layer of the glass substrate which prepared the oxide film or mixed oxide thin film which is presenting at least one or more sorts of surface configurations among the micro pit-like surface, the concave convex surface, and the convex surface as a substrate layer, and subsequently being burned by 100 - 400 \*\*.

[0015] Where membranes are formed without carrying out surface treatment to the front face of a glass substrate and this substrate, this invention Moreover, a micro pit-like surface, The substrate layer which changes with the oxide thin film or mixed oxide thin film which is presenting at least one or more sorts of surface configurations among the concave convex surface and the convex surface, On this substrate layer, at least 0.1 - 20 % of the weight of fluoro alkyl silanes, 0.04 - 2 % of the weight of particles of the tin oxide which makes antimony oxide a dopant, 0.03 - 2 % of the weight of silicone compounds, and water 0.005 - 15 % of the weight, To the mixed solution which consists of an organic solvent, it is fluoro alkyl silane 1mol about an acid. It receives and is - 5x10 to 4 mol 2x10 to 2 mol. The water-repellent glass characterized by consisting of a hydrophobic layer which is the thin film which carried out spreading membrane formation of the water-repellent oil-repellent liquid added so that it might become is offered.

[0016] Moreover, the micro pit-like surface which described this invention above on the front face of a glass substrate and this substrate, This micro pit or/and the irregularity or/, and the convex in the oxide thin film or mixed oxide thin film which is presenting at least one or more sorts of surface configurations among the concave convex surface and the convex surface R max (maximum height) =53 60nm, Rea (center line average of roughness height) = 2-20nm, A substrate [ in which the thickness which consists of their being R z(ten point average of roughness height) =5-55nm and S m(concavo-convex average spacing) =5-700nm is 10-300nm | layer, The water-repellent glass characterized by consisting of a hydrophobic layer which is the thin film which carried out spreading membrane formation of the water-repellent oil-repellent liquid described above on this substrate layer is offered. [0017] Moreover, the micro pit-like surface which described this invention above on the front face of a glass substrate and this substrate, This micro pit or/and the irregularity or/, and the convex in the oxide thin film or mixed oxide thin film which is presenting at least one or more sorts of surface configurations among the concave convex surface and the convex surface SUKYUNESU (skewness) =0 thru/or >0, KURUTOSHISU (kurtosis) = the water-repellent glass characterized by consisting of a substrate layer which consists of it being 3 thru/or >3, and a hydrophobic layer which is the thin film which carried out spreading membrane formation of the water-repellent oil-repellent liquid described above on this substrate layer is offered.

[0018] Moreover, the micro pit-like surface which described this invention above on the front face of a glass substrate and this substrate, This micro pit or/and the irregularity or/, and the convex in the oxide thin film or mixed oxide thin film which is presenting at least one or more sorts of surface configurations among the concave convex surface and the convex surface R max(maximum height) =5-60nm, R a(center line average of roughness height) =2-20nm, The substrate layer which consists of their being R z(ten-point average of roughness height) =5-55nm and S m(concavo-convex average spacing) =5-700nm, and consists of moreover it being SUKYUNESU (skewness) =0 thru/or >0, KURUTOSHISU (kurtosis) =3, or >3, The water-repellent glass characterized by consisting of a hydrophobic layer which is the thin film which carried out spreading membrane formation of the water-repellent oil-repellent liquid described above on this substrate layer is offered. [0019] Moreover, this invention is 10-300nm considering the above mentioned water-repellent oil-repellent liquid as average thickness. R max(maximum height) =5-60nm, R a(center line average of roughness height) =2-20nm, The micro pit-like surface which has the micro pit or/and the irregularity or/, and the convex which are R z(ten-point average of roughness height) =5-55nm and S m(concavo-convex average spacing) =5-700nm, It applies on the substrate layer of the glass substrate which

prepared the above mentioned oxide film or above mentioned mixed oxide thin film which becomes by at least one or more sorts in a concave convex surface and a convex surface as a substrate layer, and the manufacture approach of the water-repellent glass characterized by the ability to be burned by 100 - 400 \*\* subsequently is offered.

[0020] Moreover, the micro pit which is SUKYUNESU (skewness) =0 thru/or >0, KURUTOSHISU (kurtosis) =3, or >3 about the water-repellent oil-repellent liquid which described this invention above or/and irregularity or/, and the micro pit-like surface of a convex, It applies on the substrate layer of the glass substrate which prepared the above mentioned oxide film or above mentioned mixed oxide thin film which becomes by at least one or more sorts in a concave convex surface and a convex surface as a substrate layer, and the manufacture approach of the water-repellent glass characterized by the ability to be burned by 100 - 400 \*\* subsequently is offered.

[0021] Moreover, this invention is 10-300nm considering the above mentioned water-repellent oil-repellent liquid as average thickness. R max(maximum height) =5-60nm, R a(center line average of roughness height) =2-20nm, They are R z(ten-point average of roughness height) =5-55nm and S m (concavo-convex average spacing) =5-700nm. And SUKYUNESU (skewness) =0 thru/or >0, KURUTOSHISU (kurtosis) = The micro pit which are 3 thru/or >3 or/and irregularity or/, and the micro pit-like surface of a convex, It applies on the substrate layer of the glass substrate which prepared the above mentioned oxide film or above mentioned mixed oxide thin film which becomes by at least one or more sorts in a concave convex surface and a convex surface as a substrate layer, and the manufacture approach of the water-repellent glass characterized by the ability to be burned by 100 - 400 \*\* subsequently is offered.

[0022] As said glass substrate, it is inorganic transparence sheet glass here. It is not what can adopt the commercial soda lime glass used for the object for vehicles, the object for vessels, the object for aircrafts, or \*\*\*\*\*\*\*\*, and is limited to colorlessness or coloring and its class or a color tone, especially a configuration, etc. While being able to use it, of course as bending sheet glass with various tempered glass, on-the-strength rise glass, a plate, or the veneer, it cannot still be overemphasized that it can be used also as multiple glass or laminated glass, and glass for mirrors.

[0023] moreover, as oxide film used as the above mentioned substrate layer Although you may produce by what kind of technique, or more at least one or more sorts of two compounds are chosen, for example from a metal alkoxide system compound or a metal acetylacetonate system compound. And membranes can be formed on the basis of control of the adjustment or/and this solution of the mixed rate of two or more compounds which this this selected solution chooses of relative humidity, and it can obtain by heating at the temperature more than 100 \*\*. After membrane formation of this substrate layer considers as the gel film by for [ about 10 minutes ] order by 100 - 300 \*\*, it is desirable in order to obtain weatherability, abrasion resistance, etc. calcinating before or after for about 3 minutes excelled [ abrasion resistance ] further in abbreviation 600 \*\* order, for example, 500 - 650 \*\* extent. [0024] At least one or more sorts of surface configurations seem to become the oxide thin film which is presenting at least one or more sorts of surface configurations among the micro pit-like surface described above, without carrying out surface treatment especially, the concave convex surface, and the convex surface, and not to collapse among the micro pit-like surface at the time of coat desiccation, a concave convex surface, and a convex surface, even if it calcinates with further 550 - 650 \*\* extent. It is the same also in the following substrate layers.

[0025] About two or more selected compounds mentioned above This selection the surface of the oxide film which chose that from which average molecular weight differs, and formed membranes The shape of for example, a micro pit, The average molecular weight of two or more sorts of compounds which are for considering as concave convex or convex, and are mixed is thousands (it is specifically 800 or about 8000). It is desirable that they are 2000 thru/or about 7000 and tens of thousands (it is specifically 10000 thru/or 70000 extent) or thousands, and hundreds of thousands of (100000 thru/or about [ Specifically for example, ] 400000) combination preferably.

[0026] The sol solution A which furthermore hydrolyzed and condensed [dehydration] the metal alkoxide or metal acetylacetonate compound which has four organic functions, for example as one start

raw material as a substrate layer the sol solution B which hydrolyzed and condensed [ dehydration ] the metal alkoxide or metal acetylacetonate compound which has three organic functions or two organic functions as one more start raw material is chosen, respectively, and it mixes -- things, even if it is the sol gel film which carried out the coat of the coating solution and formed membranes It is good. [0027] by using the metal alkoxide or metal acetylacetonate compound of a dissimilar metal as a start raw material, using the sol solution C which hydrolyzed and condensed [ dehydration ], the sol solutions A and B mentioned above choose said sol solutions A and B and C at least, respectively, and are mixed further again, for example -- things -- you may be the sol gel film which carried out the coat of the coating solution and formed membranes.

[0028] Moreover, as a metal alkoxide system compound mentioned above, when only an alkoxy group combines with a metal altogether, what did not come to accept a methoxide, ethoxide, isopropoxide, etc. but the part permuted by the methyl group, the ethyl group, etc., for example, a monomethyl alkoxide, a monoethyl alkoxide, etc. are included. As a metal acetylacetonate system compound mentioned above, not only when only an acetylacetone radical combines with a metal altogether, but its part contains further again what was permuted by the methyl alkoxy group, the ethyl alkoxy group, etc. [0029] furthermore, especially as an above-mentioned metal, although it does not limit, choosing Si, Ti, or Zr as a desirable and concrete thing For example, a tetramethoxy silane [Si(OMe) 4 Me:CH3] (Following Me is CH3), A tetra-ethoxy silane [Si(OEt) 4 Et:C two H5] (Following Et is C2H5), Methyl triethoxysilane [MeSi (OEt)3] and methyl trimetoxysilane [MeSi (OMe)3], Titanium tetraisopropoxide [Ti(O-iso-Pr) 4 Pr:C three H7] (Following Pr is C3H7), Titanium acetylacetonate [Ti (CH2 COCH2 COCH3)4], Zirconium normal butoxide [Zr(O-n-Bu) 4 Bu:C four H9] (Following Bu is C4H9), Zirconium acetylacetonate [Zr (CH2 COCH2 COCH3)4] etc. is suitable. There is another dimethyl diethoxysilane [ for example, ], dimethyldimethoxysilane, titanium tetra-normal butoxide, zirconium tetra-isopropoxide, and zirconium tetra-OKUCHI rate etc.

[0030] Furthermore, as a concrete thing of the oxide film which becomes by at least one or more sorts in said micro pit-like surface, a concave convex surface, and a convex surface, or a mixed oxide thin film, the mixed oxide film of SiO2 and oxide film [ of SiO2 ], SiO2, TiO2, or ZrO2 grade etc. is mentioned. [0031] Moreover, because an expected surface configuration became is hard to be acquired in less than 10nm, maintenance of sufficient amount of water repellent became impossible and a long-term water-repellent manifestation became impossible, it was presupposed that it is 10-300nm as average thickness of the substrate layer of the oxide film which becomes by at least one or more sorts in said micro pit-like surface, a concave convex surface, and a convex surface, or a mixed oxide thin film. Moreover, when it exceeds 300nm, it is for the physical endurance of the substrate layer itself to decrease as well as becoming less economical. It is 30-200nm the optimal. It is extent.

[0032] Moreover, convex [ in the oxide thin film or mixed oxide thin film which is presenting at least one or more sorts of surface configurations among the above mentioned micro pit-like surface, the concave convex surface, and the convex surface / this shape of a micro pit, the concave convex or/, and convex ] R max(maximum height) =5-60nm, R a(center line average of roughness height) =2-20nm, That we decided to change by R z(ten-point average of roughness height) =5-55nm and S m(concavo-convex average spacing) =5-700nm Although it is difficult to express the shape of a micro pit of at least one or more sorts of surface configurations, concave convex or/, and convex among this micro pit-like surface, a concave convex surface, and a convex surface the AFM mode (the product made from the SEIKO electron, SP3700, 4-micrometer scan around, or made in Olympus --) of a scanning probe microscope R max which is the display of surface roughness [ in / it observes with NV2000 and 4 micrometer scan around, and / JIS B 0601 ], R a and R z -- further -- S m \*\*\*\* -- \*\*\*\* -- rough -- displaying -- for example, -- In R max>60nm, R a>20nm, and R z>55nm, with external stress, such as friction the shape of toothing breaks -- having -- being easy -- long-term physical endurance decreases -- in R max <5nm and R a>2nm and R z>5nm, the surface configuration which will become almost near in the shape of smooth, and expected simply aims at is because it does not become.

[0033] Furthermore, it is SUKYUNESU (Skewness=Rsk) about said shape of a micro pit, concave convex or/, and convex. Skewness =0 thru/or >0, KURUTOSHISU (Kurtosis=Rkr, kurtosis) = that we

decided to be 3 thru/or >3 It is the value as which SUKYUNESU expresses the symmetric property of the direction of longitudinal magnification in a cross-section (amplitude distribution) curve. it is machining side extent -- being the so-called -- the conic crest which sharpened above the center line from Rsk=0 many \*\* by non-flatness -- being the so-called -- It is the surface roughness of the range of Rsk>0. Since water repellent of amount sufficient in Rsk <0 [ so-called (condition which does not have a crest, so that minus is large) ] by which it is dotted with a deep trough in a flat part holds and is not made into a substrate layer, a long-term water-repellent manifestation becomes impossible. It is the desirable range of >0 comparatively near 0 thru/or 0, and the conic crest which sharpened in extent which sharpens too much thinly and physical endurance does not reduce is said surface in the condition of many \*\*(ing) by non-flatness.

[0034] Moreover, the value as which KURUTOSHISU expresses the configuration in a cross-section (amplitude distribution) curve (the thing near normal distribution is a machining side, and are Rsk=0 and Rkr=3 probability density distribution of surface roughness:) there are an unusually high crest and a deep trough where the rate for a flat part of the lateral-magnification direction is a large front face, and the crest of normal distribution sharpens too much thinly, so that a configuration is generally sharp -being the so-called -- In Rkr>3 The water-repellent manifestation of a long period of time [ \*\*\*\* / that long-term physical endurance decreases ] becomes impossible, the crest of normal distribution is moreover, low like bowl-like one widely -- it is rather dotted with the shape of a crater in-like [ flatness ] -- being the so-called -- In Rkr<3 it differs covering, while a touch area with water repellent decreases as a result and it is devoted to the cone-like crest which many \*\*, maintenance of water repellent becomes weak, and a long-term water-repellent manifestation becomes impossible -- from Rkr=3 It is the range of Rkr>3. desirable -- Comparatively close to 3 from Rkr=3 It is the range of Rkr>3 and the conic crest which sharpened moderately is said surface in the condition of flooding many \*\*(ing) by non-flatness. [0035] It is in the etched film which carries out fluoric acid processing of the oxide film from the especially conventional organic solution, for example, SiO2 film, at Rsk<0. Since water repellent of such a sufficient amount that it is set to Rkr<3, and it expects as mentioned above cannot be held on etching SiO2 film, although it is better than the case where there is no etching SiO2 film, the long-term water-repellent manifestation to aim at becomes impossible.

[0036] these things to Rsk 0 thru/or >0, and Rkr 3 thru/or >3 -- desirable -- Rsk 0 thru/or >0 comparatively near 0, and Rkr Comparatively close to 3 from Rkr =3 By being Rkr>3 Since it has surface area large as a substrate layer, the moderate depth, and a configuration, while maintenance of sufficient water repellent is possible, it has sufficient physical reinforcement to friction etc. [0037] Moreover, magnitude the shape of a micro pit in said surface, concave convex, or convex is 5 thru/or 500nm about the path by the relative humidity at the time of forming membranes, for example. It is controllable. A path is 500nm. Since the oxidation tin grain child who film reinforcement also becomes weak and makes tin oxide or antimony oxide a dopant in less than 5nm will stop being established easily on the film while the transparency of the oxide film itself is spoiled and milking if it exceeds, they are 5 thru/or 500nm. It is desirable.

[0038] Moreover, the particle size of the tin oxide particle which makes said oxidization ANCHISEN a dopant is 100nm. Since it will be hard coming to be established on the oxide film of a substrate layer, or the mixed oxide film if it exceeds, it is 100nm. The following is desirable.

[0039] As a class of fluoro alkyl silane used in this invention For example, CF3 CH2 CH2 Si (OMe)3 and CF3 CH2 CH2 SiCl3, CF3 5 (CF2) CH2 CH2 Si (OMe)3 and CF3 5 (CF2) CH2 CH2 Si(OMe) Cl3, CF3 7 (CF2) CH2 CH2 Si (OMe)3 and CF3(CF2)7 CH2 CH2 SiCl3, CF3 7 (CF2) CH2 CH2 SiMe (OMe)2 and CF3 7 (CF2) CH2 CH2 SiMe (Cl)2 etc. -- it can mention.

[0040] Moreover, as tin oxide which makes a dopant the antimony oxide used in this invention, it is HOMO (Highest Occupied Molecular Orbital) and LUMO (Lowest Unoccupied Molecular Orbital) of tin oxide. The impurity HOMO level of antimony oxide is formed between the band energy gaps of a between, and semi-conductor nature is discovered, and it uses in order to control the photodegradation of a fluoro alkyl silane. Tin oxide is cassiterite (cassiterite). It has the crystal structure, it is thought that antimony oxide exists as an interstitial solid solution in the crystal lattice, and the partial reduction of tin

oxide starts by doping antimony oxide in the crystal lattice of tin oxide (SnO2-x and Sb2O3+X). A surplus electron is supplied to the LUMO level of tin oxide, and electronic conductivity is discovered. Specifically, there are a trade name T-1 (MITSUBISHI MATERIALS CORP.) and trade name ERUKOMU (catalyst formation Industry). Moreover, as a sol containing the tin oxide particle which makes a silicon compound and antimony oxide a dopant beforehand, there is trade name ERUKOMU CT (catalyst formation Industry), for example.

[0041] Furthermore, as the above mentioned silicon compound, the hydrolyzate which used tetramethoxy [silane (OMe) Si 4] tetra-ethoxy silane Si(OEt)4] and methyl triethoxysilane [MeSi(OEt)3] and methyl trimetoxysilane MeSi(OMe) 3] as the raw material, for example is desirable. [0042] moreover -- as said organic solvent carried out -- ketones, such as ether, such as ester, such as alcohols, such as a methanol, ethanol, propanol, and a butanol, acetic-acid methyl ester, and ethylacetate ester, and diethylether, an acetone, and a methyl ethyl ketone, ethylcellosolve, etc. -- a kind -- or two or more sorts can be mixed and it can use.

[0043] Moreover, although the above mentioned acid works as a catalyst at the time of hydrolyzing a fluoro alkyl silane, a sulfuric acid, a nitric acid, a hydrochloric acid, phosphoric acid, an aromatic series sulfonic acid, an aliphatic series sulfonic acid, etc. can be used. Especially desirable things are strong acid, such as a sulfuric acid, a nitric acid, and a hydrochloric acid.

[0044] Moreover, as an amount of fluoro alkyl silanes in these above mentioned mixed solutions, it is 0.1. Since it will be hard coming to be discovered of the addition effectiveness of the tin oxide particle which the amount of fluoro alkyl silanes increases relatively to the tin oxide particle which makes antimony oxide a dopant, and makes antimony oxide a dopant if water repellence sufficient by under weight % is not acquired but it exceeds 20 % of the weight, it is 0.1 - 20 % of the weight.

[0045] Furthermore, the tin oxide particle which makes the above mentioned antimony oxide a dopant is 0.1 in order to reduce early water repellence, if it is effective in making the endurance of the water-repellent engine performance of water-repellent glass improve, and it considers as the amount, and there is no addition effectiveness at less than 0.04 % of the weight and it exceeds 2 % of the weight. Or it is 2 % of the weight.

[0046] It is 0.1 in order to reduce early water repellence further again, if the above mentioned silicon compound is required in order to make the tin oxide particle which makes antimony oxide a dopant especially stabilize and fix to an oxide film front face, and there is no addition effectiveness at less than 0.03 % of the weight as the amount and it exceeds 2 % of the weight. Or it is 2 % of the weight. [0047] Moreover, the addition of the above mentioned water is 0.005. Under by weight %, since a fluoro alkyl silane cannot fully be hydrolyzed but the amount of association to the substrate of a fluoro alkyl silane decreases, water-repellent oil repellency ability is not fully obtained. Moreover, since sufficient water-repellent oil repellency ability is not obtained since condensation will arise that a polycondensation tends to progress between fluoro alkyl silanes and a silicon compound if it exceeds 15 % of the weight, or the preservation stability of liquid falls, it is 0.005 - 15 % of the weight. [0048] The addition of an acid is fluoro alkyl silane 1mol further again. It receives and is 5x10 to 4 mol. There is no addition effectiveness at the following. 2x10 to 2 mol Since a polycondensation with fluoro alkyl silanes and a silicon compound will be promoted in a processing agent if it exceeds, since sufficient water-repellent oil repellency ability is not obtained or the preservation stability of liquid falls -- fluoro alkyl silane 1mol receiving - 5x10 to 4 mol 2x10 to 2 mol it is .

[0049] Furthermore, by applying the water-repellent oil-repellent liquid which consists of said mixed solution on the oxide film or the mixed oxide film, and drying The water-repellent oil repellency excellent in adhesion and weatherability is obtained. As desiccation baking \*\*\*\*\*\* Since the endurance of the water-repellent engine performance of water-repellent glass does not improve at the temperature exceeding under 100 \*\* or 400 \*\*, either, it is 100. Or the endurance ability which excelled [burn / it / by 400 \*\*] in the water-repellent engine performance further can be obtained. It is 150 preferably. Or it is 200 - 300 \*\* extent more preferably, and they are 350 \*\*, and stability and the thing which discovers the engine performance certainly and the becoming thing more. In addition, as the holding time, it is a 20 - 40-minute about room.

[0050] A known spreading means can adopt suitably, such as applying as the method of application further again with a brush, a cheesecloth, etc. which were absorbed with the dipping Czochralski method, the spray method, the flow coat method, the spin coat method, or the solution.

[0051]

[Function] As mentioned above, where membranes are formed without carrying out surface treatment. according to this invention, on the surface of a glass substrate Namely, the micro pit-like surface which holds a configuration as it is after baking by 550 - 650 \*\*. Oxide film or mixed oxide film which becomes by at least one sort in a concave convex surface and a convex surface, Thickness is 10-300nm. Namely, the shape of a micro pit, concave convex, Convex R max =5-60nm, R a =2-20nm, R z =5-55nm, The film concerned 0 thru/or >0, and whose chestnut TOSHISU it is S m =5-700nm, or SUKYUNESU is 3 thru/or >3 is used as the substrate layer. To the mixed solution which consists of the tin oxide, the silicon compound, the water, and the organic solvent which were distributed in the amount in which the hydrophobic layer furthermore carried out \*\*\*\*\* specification on it, and which make a fluoro alkyl silane and antimony oxide a dopant, at least By considering as the water-repellent glass which becomes by carrying out spreading membrane formation of the water-repellent oil-repellent liquid which carried out the amount addition of specification of the acid to the fluoro alkyl silane, and its manufacture approach The shape of a unique micro pit which flooding many \*\* the conic crest which sharpened moderately in the shape of [it is mainly concerned with] non-flatness, It is the surface which makes concave convex and convex, and water-repellent oil-repellent liquid excellent in preservation stability can be used, as it is devoted to the shape of a micro pit, concave convex, and convex, this sufficient quantity of water-repellent oil-repellent liquid can be held, and stability and positive membrane formation processing can be carried out to homogeneity and homogeneity. [0052] As mentioned above, when the unique substrate layer specified especially and the hydrophobic layer with the specified water-repellent oil-repellent liquid combined The contact angle 115 - 110 \*\* and 2000 hours after super JV 104 - 100 \*\*, [ an initial-contact angle ] It can clear also with these 3 person. the contact angle after 100,000 wiper rocking is 101-99 degrees -- etc. -- The water-repellent engine performance which the substrate layer led to the rise of the whole film which also contains a hydrophobic layer, of course on the strength, and was excellent in the hydrophobic layer itself, what has adhesion, is hard and shows the weatherability which excelled [things] in the water-repellent engine performance, and endurance -- becoming -- the object for vehicles, the object for vessels, the object for aircrafts, the aperture material for construction, or various products -- mirror glass etc. is resembled further markedly and it becomes useful water-repellent glass and its manufacture approach. [0053]

[Example] Hereafter, an example explains this invention concretely. However, this invention is not limited to the starting example.

[0054] Sequential washing of example 1 magnitude abbreviation 100mm x100mm and the clearance float glass substrate with a thickness of about 2mm was carried out in neutral detergent, a water rinse, and alcohol, and after drying, it wiped away with the acetone and considered as the substrate for coats. [0055] Silica sol (average molecular weight: about 3000, solid content concentration: about 30 % of the weight) about 20.0g, and silica sol (average molecular weight: about 100000, solid content concentration: about 6 % of the weight) about 28.6g are put into a beaker, and it is the solid content / solid content of high average molecular weight of low average molecular weight About 3.5 mol It considered as the ratio, diluted with about 100 isopropyl alcohol about 50g and 1-butanol g, it stirred for about 15 hours, and the coating solution was obtained.

[0056] Subsequently, membranes are formed on said glass substrate front face by the dipping method in about 23 degrees C and the environment of about 50% of relative humidity, this solution is heated for about 10 minutes by about 270 \*\*, the gel film is formed, and after grade baking and thickness are about 100nm for about 600 \*\* and about 3 minutes further about 150nm of thickness. It was extent. It is the scanning probe microscope NV2000 about the shape of surface surface type. When it measures by AFM [the microscope between atoms, scan line:256 book, scanning size:4,000nm, and Olympus Optical Co., Ltd.], as shown in Table 1 R max =23.9nm, R a =6.2nm, R z =22.1nm, S m =621nm, and its path are

about 672nm. The oxide film which presents a surface the shape of a micro pit which is the pitch diameter of about 50nm, and concave convex was obtained less than. Moreover, as O mark showed to Table 1, for SUKYUNESU (Rsk), 0 thru/or >0, and chestnut TOSHISU (Rkr) are [ the film concerned ] 3 thru/or >3 to Rsk. 0 thru/or >0 near 0, and Rkr It was set to >3 near 3 thru/or 3, and was an expected substrate layer membrane.

[0057] Further subsequently the mixed solution which mixed liquid, stirred for about 30 minutes, and had been beforehand prepared as water-repellent oil-repellent liquid by the following combination was applied on the surface thin film this shape of a micro pit, and concave convex. In addition, the presentation ratio of the water-repellent oil-repellent liquid by this example is shown in Table 2. [0058] 1g (average molecular weight: about 3000, solid content concentration:1wt%) of ethanol solutions of a silica sol, (Combination of water-repellent oil-repellent liquid) T-1[trade name: Tin oxide impalpable powder (particle size: about 20nm)]0.01g which makes a dopant the MITSUBISHI MATERIALS CORP. make and antimony oxide, Isopropyl alcohol 5.72g, 3]1g (OMe) of heptadeca tridecyl fluoro ARUKIRUSHIRAN [CF3(CF2)7CH2CH2Si, pH 1.5 nitric-acid water-solution 0.2 g, water 0.2 g, a total of 8.13g.

[0059] Water-repellent glass was obtained by drying for about 30 minutes by about 250 \*\* after that. The following trial was performed about the obtained water-repellent glass.

(Water-repellent sex test) The contact angle over the water in the inside of atmospheric air (about 25 degrees C) is measured.

[0060] (Weathering test) Super one UV estimates.

Conditions: 60 mW/cm2 The contact angle of 2000 hours after is measured.

(Abrasion resistant test) Sliding endurance with the wiper for automobiles estimates.

[0061] Conditions: While a waterworks is dropped, perform 100,000 sliding (a round trip is made into 1 time), applying the load of 105 g, and measure a contact angle.

As the result was shown in Table 2, the initial-contact angle was that in which a contact angle becomes 103 \*\*, is excellent enough, and a contact angle is excellent enough with 100 \*\* also after an abrasion resistant test also after 112 \*\* and a weathering test. The prepared water-repellent oil-repellent processing liquid is about 1 mosquito. It was the liquid enough stabilized after there are also no signs which are condensed also in a previous month and the tin oxide particle had distributed well. [0062] Silica sol about 30g of a low mean molecular weight of an example 1, and silica sol about 23.1g of a high mean molecular weight are put into the same glass substrate as example 2 example 1 at a beaker, and they are a low mean molecular weight / solid content of a high mean molecular weight About 6.5 mol Considering as the ratio, others presupposed that it is the same as that of an example 1. the obtained oxide film is shown in Table 1 -- as -- thickness -- about 50nm, R max =12.2nm, R a =3.4nm, R z =11.0nm, and S m = -- about 423nm it is -- the path of the irregularity -- about 510nm Less than and pitch diameter of about 100nm It became what has a concave convex surface including the shape of a micro pit which is extent. Moreover, the film concerned is Rsk as O mark showed to Table 1. 0 thru/or > 0 Rkr 3 thru/or > 3 to Rsk 0 thru/or > 0 near 0, and Rkr It was set to > 3 near 3 thru/or 3, and was an expected substrate layer membrane.

[0063] Further subsequently, water-repellent oil-repellent liquid was prepared by the following combination, and water-repellent oil-repellent processing was performed like the example 1 on the concave convex surface thin film including the shape of this micro pit. The presentation ratio and evaluation result of water-repellent oil-repellent liquid of this example are shown in Table 2. [0064] That is, combination of water-repellent oil-repellent liquid is ethanol solution 100 g (average molecular weight: about 3000, solid content concentration:1wt%) of a silica sol, T-1[1by trade name:MITSUBISHI MATERIALS CORP.] g, isopropyl alcohol 888 g, heptadeca tridecyl fluoro ARUKIRUSHIRAN1g, pH 1.5 nitric-acid water-solution 0.2 g, water 9.8 g, and the sum total. 1000.0 g. [0065] The initial-contact angle of the obtained water-repellent glass was what a contact angle becomes 102 \*\*, is excellent enough, and is excellent in a contact angle enough with 100 \*\* also after an abrasion resistant test also after 112 \*\* and a weathering test. The prepared water-repellent oil-repellent processing liquid was the liquid stabilized enough, and was what becomes being the same as that of an

example 1, and demonstrates the expected water-repellent engine performance.

[0066] Silica sol about 40g of a low mean molecular weight of an example 1, and silica sol about 18.2g of a high mean molecular weight are put into the same glass substrate as example 3 example 1 at a beaker, and it is about 11 mol about a low mean molecular weight / solid content of a high mean molecular weight. Considering as the ratio, others presupposed that it is the same as that of an example 1. the obtained oxide film is shown in Table 1 -- as -- thickness -- about 60nm, R max =11.1nm, R a =2nm, R z=10.0nm, and S m = -- about 358 the convex path which is convex [including the shape of a micro pit which it has ], and includes the shape of a micro pit -- about 380-500nm It became what it has. Moreover, the film concerned is Rsk as O mark showed to Table 1. 0 thru/or > 0 Rkr 3 thru/or > 3 to Rsk 0 thru/or > 0 near 0, and Rkr It was the substrate layer membrane which is set to > 3 near 3 thru/or 3, and expected aims at.

[0067] Further subsequently, water-repellent oil-repellent liquid was prepared by the following combination, and water-repellent oil-repellent processing was performed like the example 1 on the convex surface thin film including the shape of this micro pit. The presentation ratio and evaluation result of water-repellent oil-repellent liquid of this example are shown in Table 2.

[0068] That is, combination of water-repellent oil-repellent liquid is 1g (average molecular weight: about 3000, solid content concentration:1wt%) of ethanol solutions of a silica sol, T-1 [0.01by trade name:MITSUBISHI MATERIALS CORP.] g, isopropyl alcohol 2.59g, heptadeca tridecyl fluoro ARUKIRUSHIRAN1g, pH 1.5 nitric-acid water-solution 0.2 g, water 0.2 g, and a total of 5.0 g. [0069] The initial-contact angle of the obtained water-repellent glass was what a contact angle becomes 103 \*\*, is excellent enough, and is excellent in a contact angle enough with 101 \*\* also after an abrasion resistant test also after 114 \*\* and a weathering test. The prepared water-repellent oil-repellent processing liquid was the liquid stabilized enough, and was what demonstrates the water-repellent engine performance which becomes being the same as that of an example 1, and is excellent in expected.

[0070] Using the coating solution used for the same glass substrate as example 4 example 1 in the example 1, relative humidity at the time of membrane formation was made into about 35%, and others made it be the same as that of an example 1. the obtained oxide film is shown in Table 1 -- as -- thickness -- about 80nm, R max =20.2nm, R a =4.3nm, R z=18.3nm, and S m = -- about 452nm It became the shape of a micro pit and convex surface which has convex and has the micro pit whose path is about 10-20nm on a front face. Moreover, the film concerned is Rsk as O mark showed to Table 1. 0 thru/or > 0 Rkr 3 thru/or > 3 to Rsk 0 thru/or > 0 near 0, and Rkr It was the substrate layer membrane which is set to >3 near 3 thru/or 3, and expected aims at.

[0071] Further subsequently, water-repellent oil-repellent liquid was prepared by the following combination, and water-repellent oil-repellent processing was performed on this shape of a micro pit, and a convex surface thin film like the example 1. The presentation ratio and evaluation result of water-repellent oil-repellent liquid of this example are shown in Table 2.

[0072] That is, combination of water-repellent oil-repellent liquid is 1g (average molecular weight: about 3000, solid content concentration:1wt%) of ethanol solutions of a silica sol, T-1 [0.01by trade name:MITSUBISHI MATERIALS CORP.] g, isopropyl alcohol 22.59 g, heptadeca tridecyl fluoro ARUKIRUSHIRAN1g, pH 1.5 nitric-acid water-solution 0.2 g, water 0.2 g, and a total of 8.13g. [0073] The initial-contact angle of the obtained water-repellent glass was what a contact angle becomes 104 \*\*, is excellent enough, and is excellent in a contact angle enough with 100 \*\* also after an abrasion resistant test also after 114 \*\* and a weathering test. The prepared water-repellent oil-repellent processing liquid was the liquid stabilized enough, and was what demonstrates the water-repellent engine performance which becomes being the same as that of an example 1, and is excellent in expected.

[0074] the same glass substrate as example 5 example 1 -- using -- tetra-ethoxy silane [Si (OC2H5) 4:TEOS] -- 16g and ethanol (EtOH) 8.5 g and water (it adjusts to pH4 by HCl beforehand) -- 5.5 g -- heating reflux was performed at \*\*\*\* picking and about 80 degrees C for about 20 hours, respectively, and it considered as the sol solution A. It was about 40,000 when the weight average molecular weight

(Mw, polystyrene reduced property) of this sol solution A was measured. [0075] They are 36.6g and isopropyl alcohol about methyl trimetoxysilane [CH3Si(OCH3)3:MTMS]. (iPA) About 28.9g and pure water (pH7) Heating reflux was performed at 14.5g \*\*\*\* picking and about 70 degrees C for about 5 hours, and it considered as the sol solution B, the place which measured the average molecular weight of this sol solution B -- about 2,000 it was . [0076] the above-mentioned solution A and Solution B -- mixing -- iPA of about 350 g diluting -- a room temperature -- about 10 hours -- stirring -- the mole ratio of the solid content (it converts as SiO2) of Solution A and Solution B -- 1:3.5 A coating solution is obtained, it is -- by the dipping method A coat is carried out to said glass substrate front face in about 23 degrees C and the environment of about 50% of relative humidity, it heats for about 30 minutes by about 100 \*\*, and thickness is about 150nm. The gel film of SiO2 was obtained. Furthermore, for about 600 \*\* and about 3 minutes, when a surface state is observed by one about 20,000 times the scale factor [ said microscope and ] of this, as thickness is about 90nm, and it is shown in Table 1 after grade baking R max =35.5nm, R a =7.8nm, R z =33.1nm, and S m = about 657nm The shape of a micro pit and concave convex surface which has convex [ of less than 1 etc. and has an about 10-50nm diameter was made. Moreover, the film concerned is Rsk as O mark showed to Table 1. 0 thru/or > 0 Rkr 3 thru/or > 3 to Rsk 0 thru/or > 0 near 0, and Rkr It was the substrate layer membrane which is set to >3 near 3 thru/or 3, and expected aims at. [0077] Further subsequently, water-repellent oil-repellent liquid was prepared by the following combination, and water-repellent oil-repellent processing was performed like the example 1 on this shape of a micro pit, and a concave convex surface thin film. The presentation ratio and evaluation result of water-repellent oil-repellent liquid of this example are shown in Table 2. [0078] That is, combination of water-repellent oil-repellent liquid is 1g (average molecular weight: about 3000, solid content concentration:1wt%) of ethanol solutions of a silica sol, T-1 [0.16by trade name: MITSUBISHI MATERIALS CORP.] g, isopropyl alcohol 5.44g, heptadeca tridecyl fluoro ARUKIRUSHIRAN1g, pH 1.5 nitric-acid water-solution 0.2 g, water 0.2 g, and a total of 8.00g. [0079] The initial-contact angle of the obtained water-repellent glass was what a contact angle becomes 104 \*\*, is excellent enough, and is excellent in a contact angle enough with 101 \*\* also after an abrasion resistant test also after 112 \*\* and a weathering test. The prepared water-repellent oil-repellent processing liquid was the liquid stabilized enough, and was what demonstrates the water-repellent engine performance which becomes being the same as that of an example 1, and is excellent in expected.

[0080] Stirring was performed for about 30 minutes at \*\*\*\* picking and a room temperature, and tetrapropoxide [titanium (OiPr) Ti 4] 2.8 g, iPA 46.6g, and water (pH2) 0.6 g were used as Solution C at the same glass substrate as example 6 example 1. After mixing Solution A and Solution B like an example 5, this solution C was added, iPA 300 g was added further after that, and the coating solution was prepared. The mole ratio of the solid content (it converts as SiO2) of Solution A and Solution B in this coating solution and the solid content (it converts as TiO2) of Solution C is 1:3.5. : It is 0.45. SiO2 and the TiO2 mixing thin film of about 70nm of thickness were obtained like the example 5. when a surface state is observed, it is shown in Table 1 -- as -- R max = 15.8nm, R a = 4.7 nm, R z = 14.4nm, and S m = -- about 488nm Irregularity thru/or a convex surface including the shape of a micro pit which has irregularity thru/or convex and has an about 10-50nm diameter was made. Moreover, the film concerned is Rsk as O mark showed to Table 1. 0 thru/or > 0 Rkr 3 thru/or > 3 to Rsk 0 thru/or > 0 near 0, and Rkr It was the substrate layer membrane which is set to >3 near 3 thru/or 3, and expected aims at. [0081] Further subsequently, water-repellent oil-repellent liquid was prepared by the following combination, and water-repellent oil-repellent processing was performed like the example 1 on irregularity including the shape of this micro pit thru/or a convex surface thin film. The presentation ratio and evaluation result of water-repellent oil-repellent liquid of this example are shown in Table 2. [0082] That is, combination of water-repellent oil-repellent liquid is 2g (average molecular weight: about 3000, solid content concentration:1wt%) of ethanol solutions of a silica sol, T-1 [0.01by trade name: MITSUBISHI MATERIALS CORP.] g, isopropyl alcohol 46.59 g, heptadeca tridecyl fluoro ARUKIRUSHIRAN1g, 60% nitric-acid water-solution 0.2 g, water 0.2 g, and a total of 50.0g.

[0083] The initial-contact angle of the obtained water-repellent glass was what a contact angle becomes 100 \*\*, is excellent enough, and is excellent in a contact angle enough with 100 \*\* also after an abrasion resistant test also after 111 \*\* and a weathering test. The prepared water-repellent oil-repellent processing liquid was the liquid stabilized enough, and was what demonstrates the water-repellent engine performance which becomes being the same as that of an example 1, and is excellent in expected.

[0084] The mole ratio of the solid content of example 7 solutions A and B and each C is 1:11:1.2. Said substrate layer thin film of about 50nm of thickness was obtained like the example 6 except preparing a coating solution so that it may become when a surface state is observed, it is shown in Table 1 -- as -- R max =17.8nm, R a=5.3nm, R z =16.2nm, and S m = -- about 414nm Concave convex thru/or a convex surface including the shape of a micro pit which has irregularity thru/or convex and has an about 10-50nm diameter was made. Moreover, the film concerned is Rsk as O mark showed to Table 1. 0 thru/or > 0 Rkr 3 thru/or > 0 with 3 to Rsk near 0 thru/or 0, and Rkr It was the substrate layer membrane which is set to >3 near 3 thru/or 3, and expected aims at.

[0085] Further subsequently, water-repellent oil-repellent liquid was prepared by the following combination, and water-repellent oil-repellent processing was performed like the example 1 on concave convex including the shape of this micro pit thru/or a convex surface thin film. The presentation ratio and evaluation result of water-repellent oil-repellent liquid of this example are shown in Table 2. [0086] That is, combination of water-repellent oil-repellent liquid is 1g (average molecular weight: about 3000, solid content concentration:1wt%) of ethanol solutions of a silica sol, T-1 [0.01by trade name:MITSUBISHI MATERIALS CORP.] g, isopropyl alcohol 3.21g, heptadeca tridecyl fluoro ARUKIRUSHIRAN1g, pH 1.5 nitric-acid water-solution 0.2 g, 1g of water, and a total of 6.42g. [0087] The initial-contact angle of the obtained water-repellent glass was what a contact angle becomes 104 \*\*, is excellent enough, and is excellent in a contact angle enough with 100 \*\* also after an abrasion resistant test also after 114 \*\* and a weathering test. The prepared water-repellent oil-repellent processing liquid was the liquid stabilized enough, and was what demonstrates the water-repellent engine performance which becomes being the same as that of an example 1, and is excellent in expected.

[0088] In example 8 example 1, it was made to be the same as that of an example 1 except having changed combination of water-repellent oil-repellent liquid as follows.

[0089] That is, combination of water-repellent oil-repellent liquid is 1g (average molecular weight: about 3000, solid content concentration:1wt%) of ethanol solutions of a silica sol, T-1 [0.01by trade name:MITSUBISHI MATERIALS CORP.] g, isopropyl alcohol 5.59g, heptadeca tridecyl fluoro ARUKIRUSHIRAN1g, 0.11g of pH 2.1 nitric-acid water solutions, 0.29g of water, and a total of 8.00g. [0090] As the obtained water-repellent glass was shown in Table 2, the initial-contact angle was that in which a contact angle becomes 102 \*\*, is excellent enough, and a contact angle is excellent enough with 99 degrees also after an abrasion resistant test also after 113 \*\* and a weathering test. The prepared water-repellent oil-repellent processing liquid was the liquid stabilized enough, and was what demonstrates the water-repellent engine performance which becomes being the same as that of an example 1, and is excellent in expected.

[0091] In example 9 example 3, it was made to be the same as that of an example 3 except having changed combination of water-repellent oil-repellent liquid as follows.

[0092] That is, combination of water-repellent oil-repellent liquid is 1g (average molecular weight: about 3000, solid content concentration:1wt%) of ethanol solutions of a silica sol, T-1 [0.01by trade name:MITSUBISHI MATERIALS CORP.] g, isopropyl alcohol 5.59g, heptadeca tridecyl fluoro ARUKIRUSHIRAN1g, pH 1.1 nitric-acid water-solution 0.4 g, 0g of water, and a total of 8.00g. [0093] As the obtained water-repellent glass was shown in Table 2, the initial-contact angle was that in which a contact angle becomes 102 \*\*, is excellent enough, and a contact angle is excellent enough with 100 \*\* also after an abrasion resistant test also after 115 \*\* and a weathering test. The prepared water-repellent oil-repellent processing liquid was the liquid stabilized enough, and was what demonstrates the water-repellent engine performance which becomes being the same as that of an example 1, and is

excellent in expected.

[0094] In example 10 example 2, it was made to be the same as that of an example 2 except having changed combination of water-repellent oil-repellent liquid as follows.

[0095] That is, combination of water-repellent oil-repellent liquid is 0.75g (average molecular weight: about 3000, solid content concentration:1wt%) of ethanol solutions of a silica sol, T-1 [0.01by trade name:MITSUBISHI MATERIALS CORP.] g, isopropyl alcohol 22.84 g, heptadeca tridecyl fluoro ARUKIRUSHIRAN1g, pH 1.5 nitric-acid water-solution 0.2 g, water 0.2 g, and a total of 24.0g. [0096] As the obtained water-repellent glass was shown in Table 2, the initial-contact angle was that in which a contact angle becomes 104 \*\*, is excellent enough, and a contact angle is excellent enough with 100 \*\* also after an abrasion resistant test also after 112 \*\* and a weathering test. The prepared water-repellent oil-repellent processing liquid was the liquid stabilized enough, and was what demonstrates the water-repellent engine performance which becomes being the same as that of an example 1, and is excellent in expected.

[0097] In example 11 example 4, it was made to be the same as that of an example 4 except having changed combination of water-repellent oil-repellent liquid as follows.

[0098] That is, combination of water-repellent oil-repellent liquid is ethanol solution (average molecular weight: about 3000, solid content concentration:1wt%) 1.6 g of a silica sol, T-1 [0.01by trade name:MITSUBISHI MATERIALS CORP.] g, isopropyl alcohol 4.99g, heptadeca tridecyl fluoro ARUKIRUSHIRAN1g, pH 1.5 nitric-acid water-solution 0.2 g, water 0.2 g, and a total of 8.00g. [0099] As the obtained water-repellent glass was shown in Table 2, the initial-contact angle was that in which a contact angle becomes 103 \*\*, is excellent enough, and a contact angle is excellent enough with 100 \*\* also after an abrasion resistant test also after 111 \*\* and a weathering test. The prepared water-repellent oil-repellent processing liquid was the liquid stabilized enough, and was what demonstrates the water-repellent engine performance which becomes being the same as that of an example 1, and is excellent in expected.

[0100] In example 12 example 1, it was made to be the same as that of an example 1 except having changed combination of water-repellent oil-repellent liquid as follows.

[0101] namely, -- as the tin oxide which makes antimony oxide DOBANTO 1.11wt(s)% as a silicon compound sol liquid [solid content concentration 2.5 wt% of the tin oxide particle (particle size: 5nm) to which combination of water-repellent oil-repellent liquid makes antimony oxide DOBANTO -- a 1.39wt (s)% thing and a catalyst -- Formation -- make --]1g, isopropyl alcohol 5g, heptadeca tridecyl fluoro ARUKIRUSHIRAN1g, pH 2.5 nitric-acid water-solution 0.4 g, 0g of water, and a total of 7.4 g. [0102] As the obtained water-repellent glass was shown in Table 2, the initial-contact angle was that in which a contact angle becomes 102 \*\*, is excellent enough, and a contact angle is excellent enough with 100 \*\* also after an abrasion resistant test also after 113 \*\* and a weathering test. The prepared water-repellent oil-repellent processing liquid was the liquid stabilized enough, and was what demonstrates the water-repellent engine performance which becomes being the same as that of an example 1, and is excellent in expected.

[0103] In example 13 example 2, it was made to be the same as that of an example 2 except having changed combination of water-repellent oil-repellent liquid as follows.

[0104] namely, -- as the tin oxide which makes antimony oxide DOBANTO 1.11wt(s)% as a silicon compound sol liquid [solid content concentration 2.5 wt% of the tin oxide particle (particle size: 5nm) to which combination of water-repellent oil-repellent liquid makes antimony oxide DOBANTO -- a 1.39wt (s)% thing and a catalyst -- Formation -- make --]1g, isopropyl alcohol 25g, heptadeca tridecyl fluoro ARUKIRUSHIRAN1g, pH 2.5 nitric-acid water-solution 0.4 g, 0g of water, and a total of 27.4g. [0105] As the obtained water-repellent glass was shown in Table 2, the initial-contact angle was that in which a contact angle becomes 101 \*\*, is excellent enough, and a contact angle is excellent enough with 99 degrees also after an abrasion resistant test also after 111 \*\* and a weathering test. The prepared water-repellent oil-repellent processing liquid was the liquid stabilized enough, and was what demonstrates the water-repellent engine performance which becomes being the same as that of an example 1, and is excellent in expected.

[0106] [Table 1]

|      |                         |      |                       | ·            | 下          | 地層         |            | •                            |           |
|------|-------------------------|------|-----------------------|--------------|------------|------------|------------|------------------------------|-----------|
|      | 医油成<br>S:SiOz<br>T:TiOz | (nm) | 表層形状<br>N:マイクロ<br>ピット | Rmax<br>(nm) | Ra<br>(nm) | Rz<br>(nm) | Sm<br>(nm) | Rsk&Rkr<br>(0~>0.0<br>~>3-0) | 怪<br>(nm) |
| 実施到1 | S                       | 100  | M、四凸                  | 23. 9        | 6. 2       | 2 2. 1     | 621        | 0                            | 5 0       |
| 2    | S                       | 50   | M、凹凸                  | 1 2. 2       | 3. 4       | 11.0       | 423        | 0                            | 400       |
| 3    | s                       | 6 0  | м、д                   | 11. 1        | 2. 0       | 10.0       | 358        | 0                            | 400       |
| 4    | S                       | 8 0  | м, д                  | 20. 2        | 4. 3       | 18. 3      | 452        | 0                            | 3 0       |
| 5    | S                       | 9 0  | M, U                  | 35. 5        | 7. 8       | 33.1       | 657        | 0                            | 3 0       |
| 6    | S·T                     | 70   | M. U                  | 15.8         | 4. 7       | 14.4       | 488        | 0                            | 3 0       |
| 7    | s·T                     | 5 0  | N.凹凸、凸                | 17.8         | 5. 3       | 16.2       | 414        | 0                            | 3 0       |
| 8    | S.                      | 100  | M、四凸                  | 23. 9        | 6. 2       | 22. 1      | 672        | 0                            | 50        |
| 9    | S                       | 6 0  | M、凸                   | 11. 1        | 2. 0       | 10.0       | 3 5 8      | 0                            | 400       |
| 10   | S                       | 5 0  | M、凹凸                  | 12. 2        | 3. 4       | 11.0       | 510        | 0                            | 400       |
| 11   | S                       | 8 0  | M、凸                   | 20.2         | 4. 3       | 18.3       | 4 5 2      | 0                            | 3 0       |
| 12   | S                       | 100  | M、园豆                  | 23.9         | 6. 2       | 22. 1      | 672        | 0                            | 5 0       |
| 13   | S                       | 5 0  | M、EPT                 | 12.2         | 3. 4       | 11.0       | 4 2 3      | 0                            | 400       |

[0107] [Table 2]

|      |       | 潜水器油   | 夜の配合(重                   | 量%)                      |             | (m o 1)                |           | 評価                    |                        |
|------|-------|--------|--------------------------|--------------------------|-------------|------------------------|-----------|-----------------------|------------------------|
|      | 水     | 有概溶媒   | フルオロア<br>ルキルシラ<br>ン(FAS) | 酸化錫 (酸<br>化アンチモ<br>ンドープ) | シリコン化<br>合物 | FAS1モルに対<br>する酸のモル数    | 初期接触角 (*) | 耐候性試験<br>後の接触角<br>(*) | 耐摩託性試<br>験後の接触<br>角(゜) |
| 実施例1 | 4. 92 | 82.54  | 12.3                     | 0. 12                    | 0.12        | 3. 70×10 <sup>-3</sup> | 112       | 103                   | 100                    |
| 2    | 1     | 98.7   | 0. 1                     | 0. 1                     | 0. 1        | 3. 70×10 <sup>-3</sup> | 112       | 102                   | 100                    |
| 3    | 8     | 71.6   | 2 0                      | 0. 2                     | 0. 2        | 3. 70×10 <sup>-3</sup> | 114       | 103                   | 101                    |
| 4    | 1. 6  | 94.32  | 4                        | 0.04                     | 0.04        | 3. 70×10 <sup>-3</sup> | 114       | 104                   | 100                    |
| 5    | 5     | 80.38  | 12.5                     | 2                        | 0. 12       | 3. 70×10 <sup>-3</sup> | 112       | 104                   | 101                    |
| 6    | 0.005 | 86.245 | 12. 5                    | 0. 125                   | 0.125       | 5. 60×10 <sup>-3</sup> | 111       | 100                   | 100                    |
| 7    | 1 5   | 72.25  | 12.5                     | 0. 125                   | 0. 125      | 3. 70×10 <sup>-3</sup> | 114       | 104                   | 100                    |
| 8    | 5     | 82.25  | 12.5                     | 0. 12.5                  | 0.125       | 5. 10×10 <sup>-4</sup> | 113       | 102                   | 9 9                    |
| 9    | 5     | 82.25  | 1 2. 5                   | 0. 125                   | 0. 125      | 1. 90×10 <sup>-1</sup> | 115       | 102                   | 100                    |
| 10   | 1. 6  | 94.33  | 4                        | 0.04                     | 0.03        | 1. 90×10 <sup>-3</sup> | 112       | 104                   | 100                    |
| 11   | 5     | 80.38  | 12.5                     | 0.12                     | 2           | 1. 90×10 <sup>-3</sup> | 111       | 103                   | 100                    |
| 12   | 5. 4  | 80,75  | 13.51                    | 0.19                     | 0. 15       | 7. 40×10 <sup>-4</sup> | 113       | 102                   | 100                    |
| 13   | 1.46  | 94.8   | 3.65                     | 0.05                     | 0.04        | 7. 40×10 <sup>-4</sup> | 111       | 101                   | 9 9                    |

[0108] About 200 g was borrowed from the beaker and the example of comparison 1 silica sol (mean molecular weight: about 100000, solid content concentration: about 6 % of the weight) was used as the coating solution as it was. It was presupposed except it that it is the same as that of an example 1. The obtained substrate layer membrane obtained what presents the surface near a smooth side, although thickness had the shape of a micro pit about 150nm and whose front face are the pitch diameters of about 2nm. Subsequently, water-repellent oil-repellent processing liquid was prepared by the following

combination, and it gave a water-repellent finish on the substrate layer like the example 1. The compounding ratio and evaluation result of water-repellent oil-repellent liquid are shown in Table 3. [0109] That is, combination of water-repellent oil-repellent processing liquid is ethanol solution (average molecular weight: about 3000, solid content concentration:1wt%) 100 g of a silica sol, T-1[1by trade name: MITSUBISHI MATERIALS CORP.] g, isopropyl alcohol 889 g, heptadeca tridecyl fluoro ARUKIRUSHIRAN 0.5 g, pH 1.5 nitric-acid water-solution 0.2 g, water 9.8 g, and a total of 1000.5 g. [0110] It was what cannot be referred to as being what has the hydrofuge engine performance which whose expected weatherability as well as each [ said ] example to abrasion resistance is remarkably inferior unlike each [ which the contact angle became 78 degrees after the weathering test although the initial-contact angle of hydrofuge / which was obtained / oil-repellent processing glass was 100 \*\*, and it was extremely bad, the contact angle was as bad as 72 degrees also after the abrasion resistant test, and the substrate layer mentioned above by the shape of flatness | example, and is excellent at all. [0111] In the example 1 of example of comparison 2 comparison, it was made to be the same as that of the example 1 of a comparison except having changed combination of water-repellent oil-repellent processing liquid as follows. The compounding ratio and evaluation result of water-repellent oilrepellent liquid are shown in Table 3.

[0112] That is, combination of water-repellent oil-repellent processing liquid is 1g (average molecular weight: about 3000, solid content concentration:1wt%) of ethanol solutions of a silica sol, T-1 [0.01by trade name:MITSUBISHI MATERIALS CORP.] g, isopropyl alcohol 1.59g, heptadeca tridecyl fluoro ARUKIRUSHIRAN1g, pH 1.5 nitric-acid water-solution 0.2 g, water 0.2 g, and a total of 8.00g. [0113] The obtained water-repellent oil-repellent processing glass was difficult to dry, while processing, since there are few amounts of solvents, and to process the inside of a field uniformly. Moreover, although the initial-contact angle was 113 \*\* and the contact angle became 92 degrees after the weathering test, also after the abrasion resistant test, the contact angle was as bad as 78 degrees, and it was what cannot be referred to as being what has the water-repellent engine performance which is excellent in expected unlike each example which the substrate layer mentioned above according to the shape of flatness at all. About three days after it condensed, the particle of tin oxide precipitated, and this water-repellent oil-repellent processing liquid was still more unstable.

[0114] In the example 1 of example of comparison 3 comparison, it was made to be the same as that of the example 1 of a comparison except having changed combination of water-repellent oil-repellent processing liquid as follows. The compounding ratio and evaluation result of water-repellent oil-repellent liquid are shown in Table 3.

[0115] That is, combination of water-repellent oil-repellent processing liquid is 2g (average molecular weight: about 3000, solid content concentration:1wt%) of ethanol solutions of a silica sol, T-1 [0.01by trade name:MITSUBISHI MATERIALS CORP.] g, isopropyl alcohol 46.59 g, heptadeca tridecyl fluoro ARUKIRUSHIRAN1g, pH 1.5 nitric-acid water-solution 0.2 g, water 0.2 g, and a total of 50.0g. [0116] Although the initial-contact angle was 112 \*\* and the contact angle became 85 degrees after the weathering test, also after the abrasion resistant test, the obtained water-repellent oil-repellent processing glass had the contact angle as bad as 89 degrees, and was what cannot be referred to as being what has the water-repellent engine performance which is excellent in expected unlike each example which the substrate layer mentioned above according to the shape of flatness at all.

[0117] In the example 1 of example of comparison 4 comparison, it was made to be the same as that of the example 1 of a comparison except having changed combination of water-repellent oil-repellent processing liquid as follows. The compounding ratio and evaluation result of water-repellent oil-repellent liquid are shown in Table 3.

[0118] That is, combination of water-repellent oil-repellent processing liquid is 1g (average molecular weight: about 3000, solid content concentration: 1wt%) of ethanol solutions of a silica sol, T-1 [0.2 by trade name:MITSUBISHI MATERIALS CORP.] g, isopropyl alcohol 5.4 g, heptadeca tridecyl fluoro ARUKIRUSHIRAN1g, pH 1.5 nitric-acid water-solution 0.2 g, water 0.2 g, and a total of 8.00g. [0119] It was what cannot be referred to as being what has the water-repellent engine performance which compares with each example unlike each example which was as bad as 75 degrees also after the

abrasion resistant test as for the contact angle, and the substrate layer mentioned above by the shape of flatness, and the engine performance is remarkably inferior, and is excellent in expected at all by a contact angle becoming 76 degrees after a weathering test, as for the obtained water-repellent oil-repellent processing glass although an initial-contact angle is 100 \*\*.

[0120] In example of comparison 5 example 2, it was made to be the same as that of an example 2 except having changed combination of water-repellent oil-repellent liquid as follows. The compounding ratio and evaluation result of water-repellent oil-repellent liquid are shown in Table 3.

[0121] That is, combination of water-repellent oil-repellent processing liquid is 10g (average molecular weight: about 3000, solid content concentration:1wt%) of ethanol solutions of a silica sol, T-1 [0.1 by trade name:MITSUBISHI MATERIALS CORP.] g, isopropyl alcohol 59.9g, heptadeca tridecyl fluoro ARUKIRUSHIRAN10g, 60% nitric-acid water-solution 0.005 g, 0g of water, and a total of 80.005g. [0122] It was what cannot be referred to as being what has the water-repellent engine performance which a contact angle becomes 88 degrees after a weathering test, a contact angle is [ the obtained water-repellent oil-repellent processing glass ] as powerless as 88 degrees also after an abrasion resistant test although an initial-contact angle is 99 degrees, the engine performance is remarkably inferior as compared with each example, and is excellent in expected at all.

[0123] In example of comparison 6 example 2, it was made to be the same as that of an example 2 except having changed combination of water-repellent oil-repellent liquid as follows. The compounding ratio and evaluation result of water-repellent oil-repellent liquid are shown in Table 3.

[0124] That is, combination of water-repellent oil-repellent processing liquid is 1g (average molecular weight: about 3000, solid content concentration:1wt%) of ethanol solutions of a silica sol, T-1 [0.01by trade name:MITSUBISHI MATERIALS CORP.] g, isopropyl alcohol 2.81g, heptadeca tridecyl fluoro ARUKIRUSHIRAN1g, and pH1.5. Nitric-acid water-solution 0.2 g, 4g of water, a total of 9.02g. [0125] It was what cannot be referred to as being what has the water-repellent engine performance which a contact angle becomes 95 degrees after a weathering test, a contact angle is [ the obtained water-repellent oil-repellent processing glass ] as powerless as 94 degrees also after an abrasion resistant test although an initial-contact angle is 112 \*\*, the engine performance is remarkably inferior as compared with each example, and is excellent in expected at all. About one day after it condensed, the particle of tin oxide precipitated, and this water-repellent oil-repellent processing liquid was still very more unstable.

[0126] In example of comparison 7 example 2, it was made to be the same as that of an example 2 except having changed combination of water-repellent oil-repellent liquid as follows. The compounding ratio and evaluation result of water-repellent oil-repellent liquid are shown in Table 3.

[0127] That is, combination of water-repellent oil-repellent processing liquid is 1g (average molecular weight: about 3000, solid content concentration:1wt%) of ethanol solutions of a silica sol, T-1 [0.01by trade name:MITSUBISHI MATERIALS CORP.] g, isopropyl alcohol 5.59g, heptadeca tridecyl fluoro ARUKIRUSHIRAN1g, and pH2.1.0.05g of nitric-acid water solutions, 0.35g of water, a total of 8.00g. [0128] It was what cannot be referred to as being what has the water-repellent engine performance which a contact angle becomes 87 degrees after a weathering test, a contact angle is [ the obtained water-repellent oil-repellent processing glass ] as powerless as 90 degrees also after an abrasion resistant test although an initial-contact angle is 100 degrees, the engine performance is remarkably inferior as compared with each example, and is excellent in expected at all. [0129] In example of comparison 8 example 2, it was made to be the same as that of an example 2 except having changed combination of water-repellent oil-repellent liquid as follows. The compounding ratio and evaluation result of water-repellent oil-repellent liquid are shown in Table 3.

[0130] That is, combination of water-repellent oil-repellent processing liquid is 1g (average molecular weight: about 3000, solid content concentration:1wt%) of ethanol solutions of a silica sol, T-1 [0.01by trade name:MITSUBISHI MATERIALS CORP.] g, isopropyl alcohol 5.59g, heptadeca tridecyl fluoro ARUKIRUSHIRAN1g, pH1 nitric-acid water-solution 0.4 g, 0g of water, and a total of 8.00g. [0131] Although the contact angle became 97 degrees after the weathering test, the obtained water-repellent oil-repellent processing glass was as bad as 94 degrees, the contact angle compared it with

each example also after the abrasion resistant test, although the initial-contact angle was 110 \*\*, the engine performance was inferior and it was comparatively near, it was what cannot be referred to as being what has the water-repellent engine performance which is excellent in expected. About one day after it condensed, the particle of tin oxide precipitated, and this water-repellent oil-repellent processing liquid was still very more unstable.

[0132] In example of comparison 9 example 2, it was made to be the same as that of an example 2 except having changed combination of water-repellent oil-repellent liquid as follows. The compounding ratio and evaluation result of water-repellent oil-repellent liquid are shown in Table 3.

[0133] That is, combination of water-repellent oil-repellent processing liquid is 1g (average molecular weight: about 3000, solid content concentration: 1wt%) of ethanol solutions of a silica sol, T-1 [0.1 by trade name:MITSUBISHI MATERIALS CORP.] g, isopropyl alcohol 47.5g, heptadeca tridecyl fluoro ARUKIRUSHIRAN1g, and pH1.5. Nitric-acid water-solution 0.2 g, water 0.2 g, a total of 50.0g. [0134] The obtained water-repellent oil-repellent processing glass was what cannot be referred to as being what has the water-repellent engine performance which a contact angle is as powerless as 92 degrees, and whose weatherability is inferior as compared with each example, and is excellent in expected also after an abrasion resistant test by a contact angle becoming 91 degrees after a weathering test at all, although the initial-contact angle was 112 \*\*.

[0135] In example of comparison 10 example 2, it was made to be the same as that of an example 2 except having changed combination of water-repellent oil-repellent liquid as follows. The compounding ratio and evaluation result of water-repellent oil-repellent liquid are shown in Table 3.

[0136] That is, combination of water-repellent oil-repellent processing liquid is 2g (average molecular weight: about 3000, solid content concentration:1wt%) of ethanol solutions of a silica sol, T-1 [0.01by trade name:MITSUBISHI MATERIALS CORP.] g, isopropyl alcohol 4.59g, heptadeca tridecyl fluoro ARUKIRUSHIRAN1g, pH1 nitric-acid water-solution 0.2 g, water 0.2 g, and a total of 8.00g. [0137] It was what cannot be referred to as being what has the water-repellent engine performance which a contact angle becomes 90 degrees after a weathering test, the contact angle after an abrasion resistant test is [ the obtained water-repellent oil-repellent processing glass ] as powerless as 89 degrees although an initial-contact angle is 109 \*\*, the engine performance is inferior as compared with each example, and is excellent in expected at all. About three days after it condensed, the particle of tin oxide precipitated, and this water-repellent oil-repellent processing liquid was still more unstable.

[0138] In the example 1 of example of comparison 11 comparison, it was made to be the same as that of the example 1 of a comparison except having used combination of the water-repellent oil-repellent liquid of an example 1. The compounding ratio and evaluation result of water-repellent oil-repellent liquid are shown in Table 3.

[0139] It was what cannot be referred to as being what has the water-repellent engine performance which a contact angle becomes 87 degrees after a weathering test, the contact angle after an abrasion resistant test is [ the obtained water-repellent oil-repellent processing glass ] as powerless as 90 degrees although an initial-contact angle is 111 \*\*, the engine performance is inferior as compared with each example, and is excellent in expected at all.

[0140] In the example 1 of example of comparison 12 comparison, it was made to be the same as that of the example 1 of a comparison except having used combination of the water-repellent oil-repellent liquid of an example 7. The compounding ratio and evaluation result of water-repellent oil-repellent liquid are shown in Table 3.

[0141] It was what cannot be referred to as being what has the water-repellent engine performance which a contact angle becomes 92 degrees after a weathering test, the contact angle after an abrasion resistant test is [ the obtained water-repellent oil-repellent processing glass ] as powerless as 89 degrees although an initial-contact angle is 113 \*\*, the engine performance is inferior as compared with each example, and is excellent in expected at all.

[0142]

[Table 3]

|      |                                    | 下地層      |           |       | 盤木撥油液の配合 |                          | (重量%)                   |         | (mo1)               |     | 是法                     |                           |
|------|------------------------------------|----------|-----------|-------|----------|--------------------------|-------------------------|---------|---------------------|-----|------------------------|---------------------------|
|      | <b>歐化物膜</b><br>S: SiO <sub>2</sub> | 形でイクロピット | ∰<br>(nn) | ¥     | 有概容牒     | フルギロア<br>ルキルシラ<br>ン(FAS) | 戦方線 (最<br>たアンチル<br>ンドーと | シリコン化合物 | FAS1モルに対<br>する酸のモル数 | 業を  | 研集性試験<br>後の接触角<br>(* ) | <b>耐野味性成験後の被験</b><br>対し、) |
| 比較到1 | S                                  | W一H密     | 23        | 1     | 98.75    | 0.05                     | 0.1                     | 0.1     | 3. 70×10-3          | 100 | 7.8                    | 7.2                       |
| 2    | ò                                  | M-中态     | 2         | 1.0   | 64.5     | 2.5                      | 0.25                    | 0.25    | 3. 70×10-3          | 113 | 9.5                    | 7.8                       |
| က    | S                                  | W-TH     | 2         | 0.8   | 97.14    | 2                        | 0.02                    | 0.04    | 3. 70×10-           | 112 | 8.5                    | 8 9                       |
| 4    | S                                  | M-中海     | 2         | 5     | 79.88    | 12.5                     | 2.5                     | 0.12    | 3. 70×10-3          | 100 | 7 6                    | 7.5                       |
| ß    | တ                                  | M, 1012  | 400       | 0.003 | 87.247   | 12.5                     | 0. 125                  | 0. 125  | 2. 80×10-3          | 6 6 | 80 80                  | 8 8                       |
| 9    | S                                  | M, 102   | 400       | 2 0   | 67.25    | 12.5                     | 0. 125                  | 0. 125  | 3. 70×10-3          | 112 | 9.5                    | 9.4                       |
| 7    | S                                  | M, 때가    | 400       | 5     | 82.25    | 12. 5                    | 0.125                   | 0. 125  | 2. 30×10-4          | 100 | 8.7                    | 9.0                       |
| 8    | S                                  | M、매과     | 400       | ŝ     | 82.25    | 12.5                     | 0. 125                  | 0. 125  | 2. 40×10-1          | 110 | 9.7                    | 9.4                       |
| 6    | S                                  | M、配      | 400       | 0, 8  | 86.98    | 2                        | 0.2                     | 0.02    | 1. 90×10-1          | 112 | 9.1                    | 9.2                       |
| οί   | Ø                                  | M、四凸     | 400       | 5     | 19.88    | 12.5                     | 0.12                    | 2. 3    | 1. 90×10-3          | 109 | 0 6                    | 6.8                       |
| 11   | S                                  | 安計────   | . 2       | 4.92  | 82.54    | 12.3                     | 0.12                    | 0.12    | 3. 70×10-3          | 111 | 8.7                    | 9.0                       |
| 12   | S                                  | 架計—W     | 2         | 1.5   | 72.25    | 12. 5                    | 0. 125                  | 0.125   | 3. 70×10-1          | 113 | 9.2                    | 6 &                       |

# [0143]

[Effect of the Invention] As described above, according to the water-repellent glass of this invention, and its manufacturing method A unique coat can be easily obtained efficiently cheaply by easy film means forming as the specified water-repellent oil-repellent liquid excellent in preservation stability is also. It becomes what is excellent in water repellence, membraneous quality, adhesion, hardness, weatherability, etc. in the long run, without spoiling an optical property. Weatherability and abrasion

resistance excellent in the especially marked water-repellent engine performance shall be shown, the object for construction or the aperture material for automobiles is begun, and useful water-repellent glass employable suitable for various glass goods etc. and its manufacture approach are offered.

[Translation done.]